



NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

A THREE-DIMENSIONAL TRANSONIC, POTENTIAL FLOW
COMPUTER PROGRAM, ITS CONVERSION TO IBM
FORTRAN AND UTILIZATION

by

Jack Paschall III

December 1983

Thesis Advisor:

R. D. Zucker

Approved for Public Release, Distribution Unlimited

T215666

REPORT DOCUMENTATION PAGE

READ INSTRUCTIONS
BEFORE COMPLETING FORM

1. REPORT NUMBER		2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) A Three-Dimensional Transonic, Potential Flow Computer Program, Its Conversion to IBM Fortran and Utilization			5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; December 1983
7. AUTHOR(s) Jack Paschall III			6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943			8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943			10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)			12. REPORT DATE December 1983
			13. NUMBER OF PAGES 152
			15. SECURITY CLASS. (of this report) UNCLASSIFIED
			15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for Public Release, Distribution Unlimited			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Computer Program; Inviscid, Three-Dimensional Transonic Potential Flow Over Wings or Wing-Body Combinations			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This thesis describes the conversion of a computer program from Fortran IV for the NOS 1.2 operating system of the CYBER 175 or CDC 6600 computer to Fortran IV compatible with the Naval Postgraduate School IBM 3033 system. The converted program, called FLO27, calculates the inviscid, three-dimensional transonic potential flow over wings or wing-body combinations. The data input to FLO27 is			

extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

Approved for Public Release, Distribution Unlimited

A Three-Dimensional Transonic, Potential Flow Computer
Program, Its Conversion to IBM Fortran and Utilization

by

Jack Faschall III
Commander, United States Navy
B.S., Oregon State University, 1965

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
December 1983

ABSTRACT

This thesis describes the conversion of a computer program from Fortran IV for the NOS 1.2 operating system of the CYBER 175 or CDC 6600 computer to Fortran IV compatible with the Naval Postgraduate School IBM 3033 system. The converted program, called FLO27, calculates the inviscid, three-dimensional transonic potential flow over wings or wing-body combinations. The data input to FLO27 is extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

TABLE OF CONTENTS

I.	INTRODUCTION	9
	A. BACKGROUND	9
	B. VISCOUS/INVISCID SYSTEM OF PROGRAMS	10
II.	POTENTIAL FLOW PROGRAM FLO27	14
	A. RE-PROGRAMING	14
	B. PROGRAM DESCRIPTION	19
	1. Program Input	22
	2. Program Output	32
III.	INTERACTIVE INPUT PROGRAM FLO27IN	35
IV.	FLO27 BATCH SYSTEM EXECUTION	38
V.	PROGRAM TEST RESULTS	40
	A. ACCEPTANCE TEST DATA	40
	B. COMPARISON WITH OTHER PROGRAMS	41
	C. AE-4501 CLASS PROJECT	41
	APPENDIX A	44
	APPENDIX B	46
	APPENDIX C	47
	APPENDIX D	48
	APPENDIX E	70
	APPENDIX F	132
	LIST OF REFERENCES	151
	INITIAL DISTRIBUTION LIST	152

LIST OF TABLES

I.	Viscous/Inviscid Wing System of Programs	11
II.	CDC Magnetic Tape Files	15
III.	FLO27 Re-Programing Changes	16
IV.	Initialized Input Variables	18

LIST OF FIGURES

1.1.	Viscous/Inviscid Interaction Procedure	12
2.1.	Dihedral Angle	27
2.2.	Wing Defining Geometry	28
2.3.	Section Defining Geometry	31
2.4.	Versatec Plot of C_p vs. X/C	34
5.1.	Program Calculated and Wind Tunnel Data	42

ACKNOWLEDGEMENT

I would like to acknowledge the most valuable assistance of the W. R. Church computer center personnel in the successful completion of this thesis. In particular, the guidance of Mr Dennis Mar was instrumental in directing my initial efforts. I am grateful to Dr Robert Zucker for providing the constant attention and encouragement which kept me working at an even pace. In addition, I am deeply appreciative of the love and support provided by my wife Tricia and our two children. Most of all I thank God for the strength, determination and peace which has sustained me and brought this project to a successful completion.

I. INTRODUCTION

In the Aeronautical Engineering curriculum graduate level aerodynamics course, AE-4501, the students are exposed to two computer programs. One of these, prepared by the Douglas Aircraft Company, analyzes the potential flow around three-dimensional wings but is limited to incompressible flow [Ref. 1]. The other program, prepared by Cebeci, calculates the friction drag for two dimensional incompressible flow over airfoils [Ref. 2]. A serious defect of these programs is that they are not state-of-the-art computer programs. The Douglas program does not consider the effects of compressibility and the boundary layer program, in addition to being restricted to incompressible flow, does not predict the laminar to turbulent transition point.

A. BACKGROUND

In 1980 the Department of Aeronautics at the Naval Postgraduate School acquired an intricate computer program recently developed by the Boeing Commercial Airplane Company. This state-of-the-art program calculates three-dimensional transonic flow over wings and bodies in

both the outer-inviscid flow region governed by the transonic potential equation and the thin layer in which the first order, compressible boundary layer equations are assumed to be valid.

The Boeing program as received was designed to be executed on a CDC 6600 or a CYBER 175 computer and was written using CDC FORTRAN IV extended language. This thesis therefore was primarily concerned with the conversion of the program to FORTRAN IV extended compatible with the Naval Postgraduate School's (NPS) IBM 3033 system. The large modular program was divided so that the potential flow analysis portion could be run separately. Simplified instructions for use of the program were also prepared.

B. VISCOUS/INVISCID SYSTEM OF PROGRAMS

The Viscous/Inviscid Wing System (VIWS) of programs calculates three-dimensional transonic flow over wings and wing body combinations including details of the laminar or turbulent flow in the three-dimensional viscous boundary layer. The flow field is calculated in two overlapping regions: an outer inviscid flow region governed by the transonic potential equation, and a thin boundary layer in which the first order, three-dimensional, compressible

boundary layer equations are assumed to hold and in which the effects of surface heat and mass transfer can be computed. A list of the VIWS of programs is presented in Table I.

TABLE I

Viscous/Inviscid Wing System of Programs

Program Name	Description
F1027	Jameson-Caughey inviscid, transonic wing code
A411IN	Reads geometry & velocity data, constructs coordinate system
VWIN	Potential flow boundary layer interface
A411AC1	Three-dimensional boundary layer program
INTERP	Boundary layer potential flow interface
A411F1 A411P2 A411FS	Graphics display programs

The basic sequence of calculations used by the VIWS to obtain matched viscous and inviscid solutions consists of an iterative loop in which the inviscid outer flow analysis and the boundary layer analysis are performed sequentially. The iterative sequence is continued until either convergence (satisfactory matching) is achieved, or the maximum number of iterations specified by the user has been performed. The VIWS programming sequence is shown schematically in Fig. 1.1.

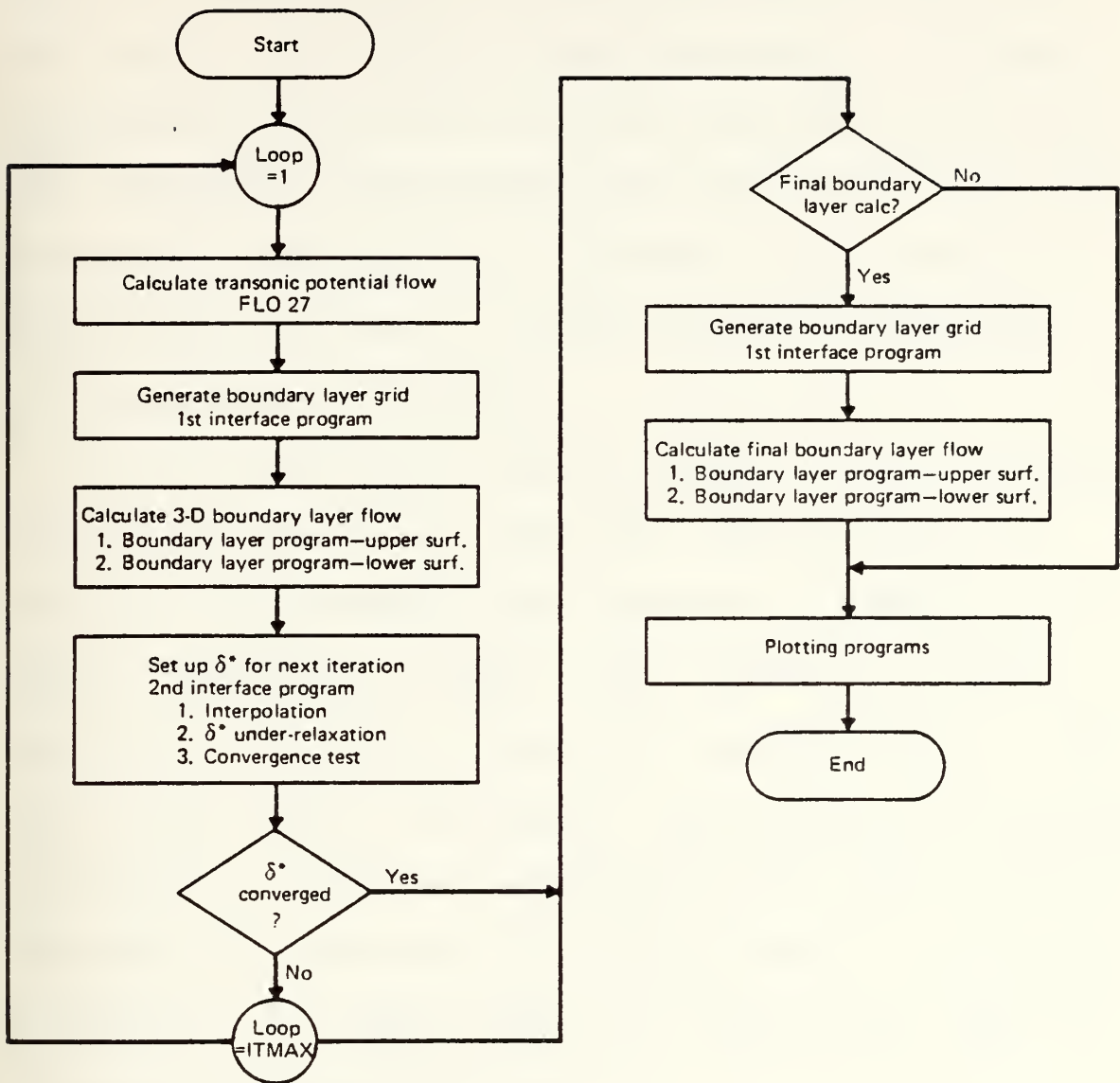


Figure 1.1. Viscous/Inviscid Interaction Procedure

The potential flow is calculated for the bare wing during the first iteration. In subsequent iterations, the effect of the boundary layer flow on the outer inviscid flow is

felt as a modification to the wing shape through the addition of the boundary layer displacement thickness. Convergence is recognized, and the iterations are stopped, when the maximum change between the new and old displacement thickness, expressed as a fraction of the maximum displacement thickness, is less than the convergence tolerance chosen by the user.

The VIWS utilizes the Jameson-Caughey transonic inviscid wing program FLO27, to carry out the potential flow analysis. The boundary layer analysis is performed by a finite difference boundary layer prediction program developed by the Boeing Commercial Airplane Company. The basic theory behind the boundary layer program is contained in [Ref. 3]. A detailed description of the VIWS of programs (excluding the potential flow program FLO27) is contained in [Ref. 4]. A basic guide to the use of the VIWS of programs is contained in [Ref. 5].

II. POTENTIAL FLOW PROGRAM FLO27

Because of the extensive length and number of program modules in the VIWS, the Potential Flow Program, FLO27, was singled out for conversion. It was anticipated that FLO27 would be run separately at first and recombined with the other program modules at some later date when these modules were themselves translated for execution on the IBM 3033 computer.

A. RE-PROGRAMING

The Potential Flow Program, hereafter called FLO27, was received on magnetic tape and loaded into the IBM 3033 mass storage system using the Job Control Language (JCL) routines presented in Appendix A. The magnetic tape contained twenty (20) total files in which the format was 9 track, 1600 CPI, unlabeled. The card image format for the sixteen (16) program files is 80 characters per record and the four (4) output files contain 150 characters per record. The program and output files on the original CDC tape are listed in Table II.

The FLO27 program was converted to FORTRAN IV extended suitable for execution on the IBM computer using the NPS CDC

TABLE II

CDC Magnetic Tape Files

File/Records	Name	Description
1 / 2356	FLO27	Potential Flow Program
2 / 3194	A411IN	Reads geometry & velocity data constructs coordinate system
3 / 378	VWIN	Potential flow boundary-layer interface
4 / 6611	A411AO1	Three-dimensional boundary layer program
5 / 1977	INTERP	Boundary-layer potential flow interface
6 / 688	A411PS	Streamline plots
7 / 211	A411P1	One-dimensional plots
8 / 586	A411P2	Contour plots
9 / 70	COUPLE	Procedure files
10 / 158	ITER	
11 / 7	DATAIN	
12 / 78	FINAL	
13 / 434	BOEB1	Boeing McLean computer program
14 / 36	CONTPLT	Contour plots
15 / 17	CORDPLT	One-dimensional plots
16 / 40	STREPLT	Streamwise plots
17	OUTF27	Output from FLO27
18	OUTIFC	Output from VWIN
19	OUT411L	Output from boundary-layer, lower surface
20	OUT411U	Output from boundary-layer, upper surface

to IEM conversion guide [Ref. 6]. The first step taken consisted of program compilation using the WATFIV compiler with its extended error messages. The listing which was

produced flagged all areas of the program which required revision. Program changes were accomplished utilizing this WATFIV listing. Some of the more general and repetitive changes are listed in Table III.

TABLE III

FLO27 Re-Programming Changes

CDC Code	IBM Code Change
Variables: FREAD, FREAF, FWRIT, FWRIF, IREAD, IREAF, IWRIT, IWRIF	Eliminated from program
WRITE(IWRIT,600)	WRITE(6,600)
READ(IREAF,500)	READ(5,500)
READ 7, WRITE 7 or REWIND 7	Changed to READ 14, WRITE 14 or REWIND 14
Call SECCND(T)	Step eliminated
Call SSWITCH(1,ISTOP)	Call SLITET(1,ISTOP)
Delimiter of form *	Replaced by '
Comment cards with *	Replaced by C
LEVEL statement	Step eliminated
If(UNIT(N).GT.0.) GO TC	All of this type eliminated

The most difficult change to make occurred with the CDC Buffer IN or Buffer OUT statements which were used in the program to transfer portions of a three-dimensional array into and out of main memory. The Buffer routines reduce the memory size required to execute the program. This statement type occurred in the main program and several of the subroutines.

The change required to translate this statement is presented below with the CDC code preceding the IBM FORTRAN.

BUFFER OUT (N3,1) (G(1,1,1),G(MX,MY,1)) changed to

WRITE(N3) ((G(I,J,1),I=1,MX),J=1,MY) and

BUFFER IN (N1,1) (G(1,1,M),G(MX,MY,M)) changed to

READ(N1,ERR=) ((G(I,J,M),I=1,MX),J=1,MY)

The variable ERR was assigned the GO TO statement number of the UNIT statement immediately following the BUFFER IN line of code. As an example, if the UNIT statement following the BUFFER IN code was - If(UNIT(N1).GT.0.) GO TO 151, then the number 151 was assigned to variable ERR following the equal sign. All CDC UNIT statements were eliminated from the FLO27 source code per Table II.

In addition to the program changes required to run FLO27 on the IBM computer, several lines of code were added to modify the output format to a more usable form. A subroutine, VERTEC, which calls the Versatec plotter was also added to enhance program usefulness. This plotting routine is user controlled through an input variable and is explained in the next section. The modified FLO27 program source code is presented in Appendix E.

To facilitate program data entry several input variables which had recommended values were initialized to these values within the Main program and the subroutine GEOM. The initialized input variables and their values are presented in Table IV.

TABLE IV
 Initialized Input Variables

AREA	VARIABLE NAME	INITIALIZED VALUE
MAIN Prgm.	XSCAL	0.0
	PSCAL	0.0
	FCONT	0.0
	P20	0.7
	P30	1.0
	FSMCO	0.0
	PTMAP	0.0
	BLCP	0.0
	WEIG	1.0
	PTCK	0.0
	FIX	0.0
	YSYM	0.0
Subrt. GEOM	FNB	2.0
	PX	0.0
	PZ	0.0
	TRL	0.0
	SLT	0.0
	XSING	0.0
	YSING	0.0

A complete description of each input variable in Table IV can be found on pages 19 through 23 of [Ref. 5].

B. PROGRAM DESCRIPTION

The FLC27 program is a computer code written to analyze the transonic flow over a wing alone or a wing on a cylindrical fuselage. It uses a finite-volume formulation to solve the exact potential flow equation in conservative form. In the development of the equations, the basic assumptions are; steady flow, no heat or work transfer, isentropic flow, irrotational flow, no body forces and a perfect gas. The velocity vector in cartesian coordinates is

$$\vec{V} = u\hat{i} + v\hat{j} + w\hat{k} \quad (2.1)$$

where u , v and w are the velocity components. The continuity equation, assuming steady flow, is

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) + \frac{\partial}{\partial z}(\rho w) = 0 \quad (2.2)$$

Next a velocity potential is introduced such that the velocity components are calculated as the gradient of this potential.

$$u = \phi_x, \quad v = \phi_y, \quad w = \phi_z \quad (2.3)$$

With the introduction of the velocity potential, the continuity equation 2.2 becomes

$$\frac{\partial}{\partial x}(\rho \phi_x) + \frac{\partial}{\partial y}(\rho \phi_y) + \frac{\partial}{\partial z}(\rho \phi_z) = 0 \quad (2.4)$$

Assuming no heat or work transfer, the energy equation can be written as

$$T \left[1 + \frac{(\gamma - 1)}{2} M^2 \right] = T_\infty \left[1 + \frac{(\gamma - 1)}{2} M_\infty^2 \right] \quad (2.5)$$

The flow is assumed to be uniform in the far field. On the surface of the body, the normal velocity component is zero. The velocities and densities of the near field are normalized using the free stream velocity and density, thus $V_\infty = 1$ and $\rho_\infty = 1$. Using the assumptions that the flow is isentropic and a perfect gas, the energy equation 2.5 can be shown to be

$$\rho = \left[1 + \frac{(\gamma - 1)}{2} M_\infty^2 (1 - v^2) \right]^{-\frac{1}{\gamma - 1}} \quad (2.6)$$

With equations 2.5 and 2.6 there are only two unknowns, ϕ and ρ . They can be solved, subject to the boundary condition of flow tangency, using a finite volume technique. The basic numerical scheme for the solution is the

construction of a mesh from small volume elements (cubes) which are packed around the wing or wing body configuration. The cubes in the computational domain are separately mapped to distorted cubes in the physical domain by independent transformations from local coordinates X , Y and Z to Cartesian coordinates x , y and z . The mesh points are the vertices (corners) of the mapped cubes. The velocity potential and density are calculated at each vertex in the mesh. The pressure distribution can then be calculated from

$$P = \frac{\rho^\sigma}{\gamma M_\infty^2} \quad (2.7)$$

In the event that the local flow velocity becomes supersonic and shocks occur, these are handled in the usual manner by insuring that:

- 1) The tangential velocity components are equal on each side of the shock.
- 2) Continuity is maintained by keeping the product of ρU_n constant across the shock (where U_n is the normal velocity component).
- 3) Discontinuous expansions (corresponding to an "expansion shock") are excluded from the flow field.

The assumption of isentropic flow along with the existence of shocks presents a contradiction which can only be resolved by limiting the flow to very weak shocks for which entropy and vorticity generation may be ignored. Thus, solutions will be valid only for subsonic free stream velocities.

The main three-dimensional array containing the potential function data is stored on disk, and special unformatted input/output statements are used to bring planes of data into central computer memory and to store updated planes of data back on the disk. In the construction of the computational coordinate system, a Joukowski transformation is used to transform the cylindrical fuselage to a vertical slit and then a sheared parabolic transformation is used in planes containing the airfoil sections. A detailed mathematical formulation of the potential flow analysis is contained in [Ref. 7].

1. Program Input

The input to FLO27 consists of variables which are read with an 8F10.6 FORMAT. Each input card has a title card which precedes it. This title card contains the input variable name and effectively labels the input data for easy

reference. The title for each input data is placed in the same column as the input data it labels. The title cards are read with a 20A4 FORMAT. All numerical input values are real numbers. The following data deck, listed card by card, is the minimum input data required for a simple wing analysis. Each "card" can be interpreted as one line of data on your terminal. A complete sample data set is presented in Appendix C.

CARD 1 The Run Title (64 characters maximum)

CARD 2 Title card for the input variables
FNX, FNY, FNZ, FMESH and FPIOT

CARD 3

Cols. 1-10 FNX - Number of computational cells in the chordwise direction for the initial mesh.

MAX = $160/2**n$, where $n = FMESH - 1$. (See Cols. 31-40 for FMESH)

Cols. 11-20 FNY - Number of computational cells in the normal direction from the airfoil surface for the initial mesh.

MAX = $16/2**n$, where $n = FMESH - 1$.

Cols. 21-30 FNZ - Number of computational cells in the spanwise direction for the initial mesh.

MAX = $32/2**n$, where $n = FMESH - 1$.

Cols. 31-40 FMESH - Determines the number of times a program generated computational mesh is refined. Enter only 1.0, 2.0 or 3.0 for coarse, medium or fine mesh. If 3.0 is selected the program will calculate flow over the wing for the coarse mesh then half the mesh size (medium), recalculate, then half the mesh again (fine) and do a final potential flow calculation. Output parameters are printed for each mesh size for which calculations were performed.

Cols. 41-50 FELOT - Output flag

0.0 = Normal output without printer-plot of Cp

1.0 = Normal output with printer-plot of Cp at each computational mesh point for each wing section.

2.0 = Normal output with Versatec plots of Cp versus X/C for each wing section of the final mesh.

CARD 4 Title card for the input variables

FIT, COVO and P10

CARD 5-M One card for each computational mesh. Total number of cards equal to $M = FMESH$.

Cols. 1-10 FIT - A parameter which fixes the maximum number of iterations the program will use to converge the velocity potential to a specified tolerance (COVO). This parameter must be repeated for each mesh refinement.

Cols. 11-20 COVO - Velocity potential convergence criteria. This input variable is also entered for each selected mesh. A value of 0.000001 is recommended.

Cols. 21-30 P10 - This parameter determines the subsonic point relaxation factor for the specified mesh size. A value of less than 2.0 must be entered for each designated mesh. Recommended values are: 1.6 for coarse, 1.3 for medium and 1.2 for the fine mesh.

CARD 6 Title card for the input variables

FMACH, YA, AL and CDO

CARD 7

Cols. 1-10 FMACH - Free stream Mach number

Cols. 11-20 YA - Yaw angle in degrees

Cols. 21-30 AL - Angle of attack in degrees

Cols. 31-40 CDO - Drag coefficient due to skin friction. Unless known, an estimated value of 0.01 is recommended.

CARD 8 Title card for the input variables

ZSYM, FNS, SWEEP, DIHED and FUS

CARD 9

Cols. 1-10 ZSYM - The wing planform symmetry trigger.

0.0 = Yawed wing, has no spanwise symmetry

1.0 = Swept wing, has spanwise symmetry

Cols. 11-20 FNS - This input variable tells the program the total number of wing sections you have selected to define the wing half span. The number must be at least three (3) but not more than eleven (11) sections.

Cols. 21-30 SWEEP - Leading edge sweep angle in degrees.

Cols. 31-40 DIHED - Dihedral angle in degrees. See

Fig. 2.1.

Cols. 41-50 FUS - Input the fuselage radius. Enter 0.0 for a wing-alone case.

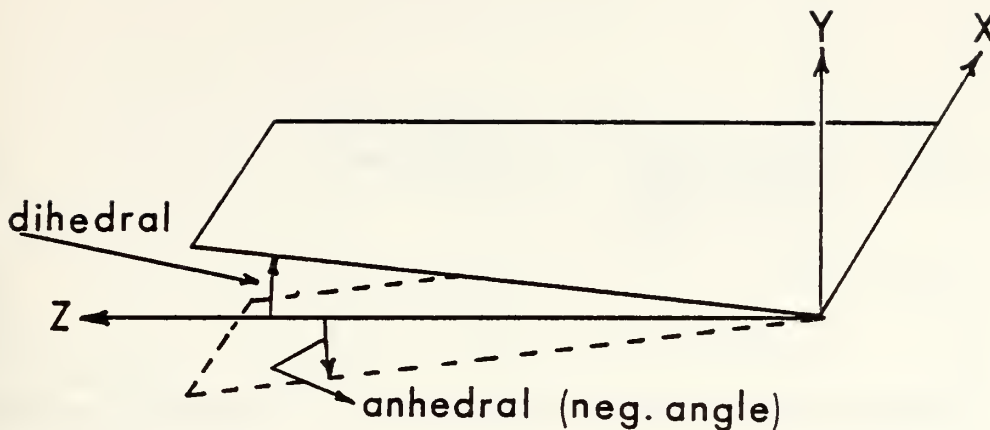


Figure 2.1. Dihedral Angle

Data input cards from 10 through 15 are used for defining wing planforms and section geometrics. For the first wing section, all data cards from card 10 through card 15 must be used. For the second and subsequent sections there is an option for skipping the wing section defining data (cards 12 through 15) and copying the data from that of the previous section. This option is controlled by the input variable FSEC. If this option is not used, data cards from 10 through 15 must be repeated for each wing defining section. The number of wing sections which are defined is input with the variable FNS. Remember, up to 11 sections may be defined, and a minimum of 3 sections must be defined. All wing planform and section defining geometrics must be in consistent units. Wing planform and section defining quantities are presented in Fig. 2.2.

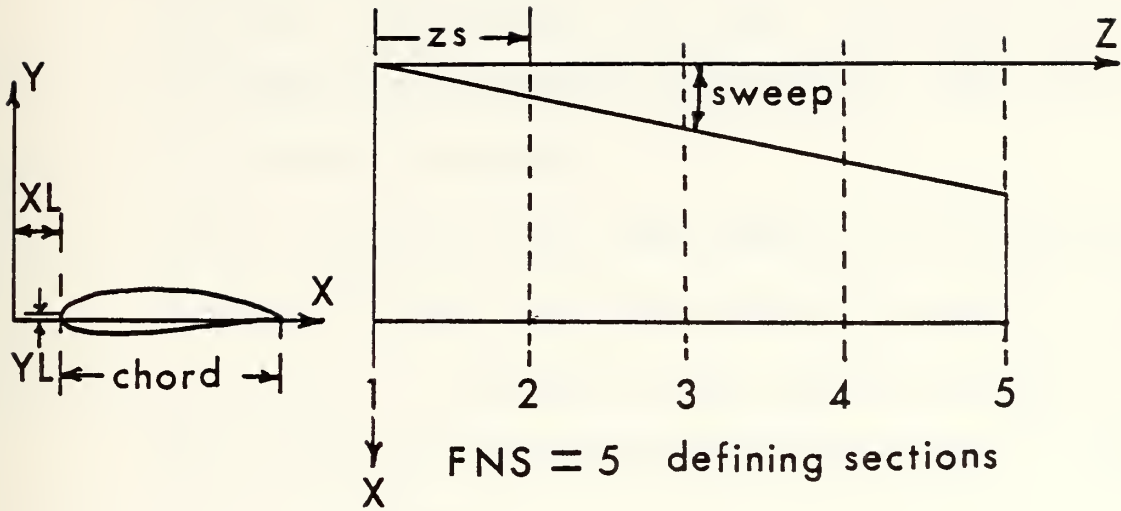


Figure 2.2. Wing Defining Geometry

CARD 10 Title card for the input variables

ZS, XI, YL, CHORD, THICK, AT and FSEC

CARD 11

Cols. 1-10 ZS - The section spanwise coordinate
 (Start at the centerline and work
 outboard)

Cols. 11-20 XL - Section leading edge X coordinate

Cols. 21-30 YL - Section leading edge Y coordinate

Cols. 31-40 CHORD - Section chord length

Cols. 41-50 THICK - The thickness scaling factor can be used to scale all Y coordinates of the wing section. Thus percent thickness and camber are increased (or decreased) accordingly. Use 1.0 if no scaling is desired.

Cols. 51-60 AT - The twist angle of each section (geometric twist) measured from the X axis to the chord line. A positive twist angle reduces the section angle of attack and gives "washout". Use 0.0 for no twist.

Cols. 61-70 FSEC - This is a flag which determines whether or not the program reads wing section defining geometry from a previous wing section or from new defining geometry. For the first section defined you must set FSEC to 1.0. Following the first section, if you define new section geometry then use FSEC = 1.0. If you want the program to read the section geometry defined from the previous section then set FSEC = 0.0.

CARD 12 Title card for the input variable

FN

CARD 13

Ccls. 1-10 FN - This variable contains the number of points which define the upper and lower surface of the section. A maximum of 161 points may be used.

CARD 14 Title card for the input variables

XF(I) and YP(I)

CARDS 15-1 to 15-N Total number of cards equals N,

where $N = \text{integer part of } (FN+2)/3.$

The X and Y coordinates at each point are entered in pairs, three points to a card. (See Appendix C for sample input)

Ccls. 1-10 XP(I) - X coordinate of the wing
section point

11-20 YP(I) - Y coordinate of the wing
section point

21-30 defining X coordinate for next
point

31-40 defining Y coordinate for next
point

41-50 defining X coordinate for
following point

defining Y coordinate for
following point

The X and Y coordinates of the wing section defining points must be entered starting with the upper surface trailing edge point and proceeding along the upper surface to the leading edge, and returning along the lower surface to the lower surface trailing edge point. It is very important to define the section leading edge with a large number of closely spaced points. Suggest at least 0.05 spacing or less between X coordinate values from 0.1 X/C to the leading edge, $X/C = 0.0$. Each X and Y coordinate point is normalized using the chord length for that section. Section defining geometrics are illustrated in Fig. 2.3.

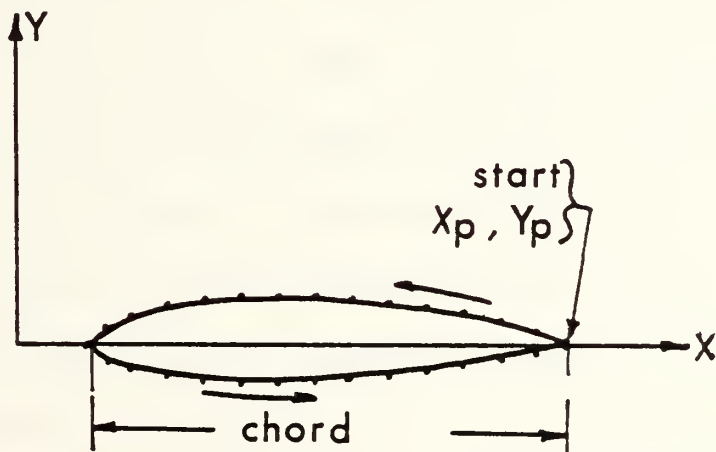


Figure 2.3. Section Defining Geometry

CARD 16 Title card containing the words in Cols. 1-80

END OF CALCULATIONS

CARD 17 Title card for the input variable

FNX

CARD 18

Cols. 1-10 FNX - This variable indicates the end of a set of calculations and must be set equal to 0.0. Its purpose is to indicate that the program has run to completion.

2. Program Output

Output from the FLO27 program varies with the value of the input variable FPLCT. When FPLCT is set equal to 0.0 a normal output is produced. This normal output contains (in order of occurrence): refined input geometry data including trailing edge slope and angle calculations; iterative solution of the potential flow mesh; section characteristics and wing characteristics. The iterative solution, section and wing characteristic data are repeated for each mesh refinement requested. Thus, if the input variable FMESH is set equal to 3, these data are calculated and output three times. The last data in the normal output consists of the non-dimensionalized chord (X/C) and pressure

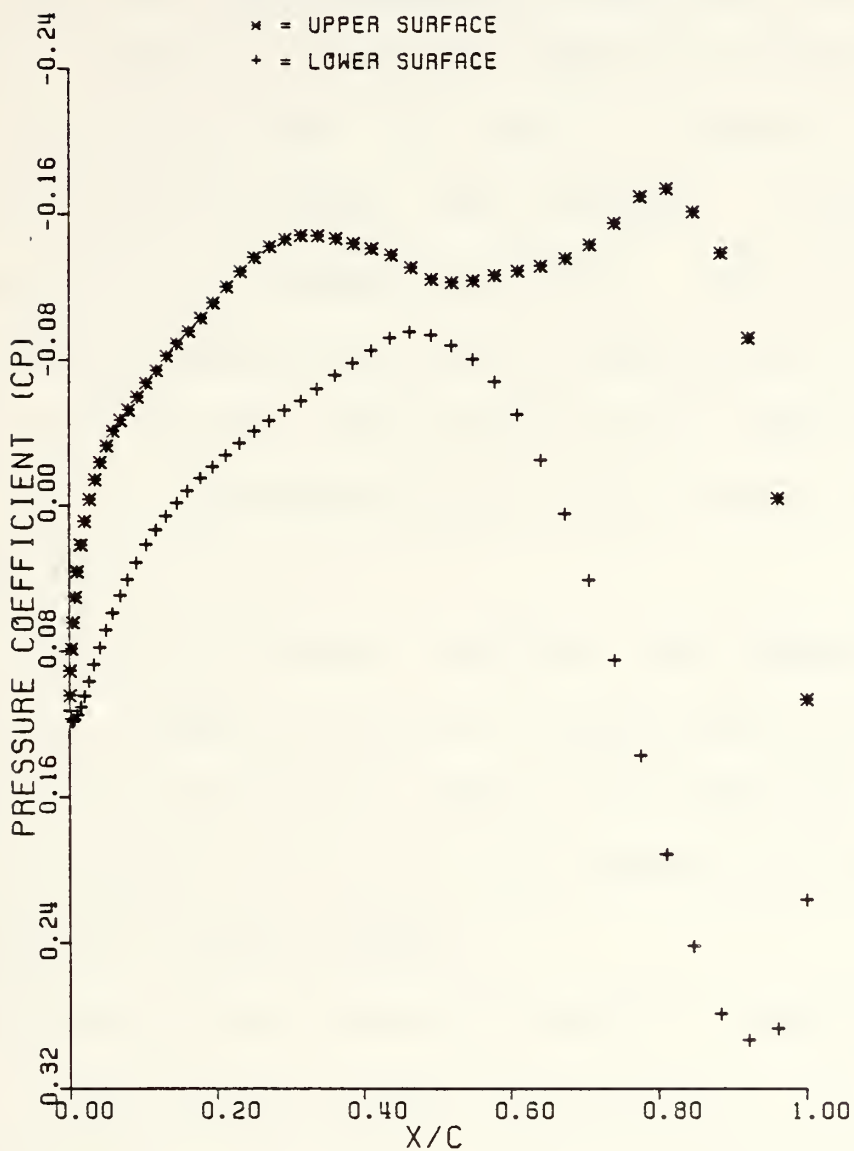
coefficient (C_p) data at each computational mesh point for each wing section calculated during the final mesh. A sample of the normal output data is presented in Appendix D and represents the output data from Appendix C input data.

If variable FPLOTT is set equal to 1.0, the output data is increased considerably. This output contains the normal output plus a line printer-plot of the pressure coefficient at each computational mesh point for each wing section. The line printer-plot is produced for each wing section of each mesh refinement. The length of the output data with FPLOTT set equal to 1.0 can approach 6000 records depending on the number of mesh refinements requested. These plots are of questionable value and, therefore, an alternate plotting program was developed.

When the variable FPLOTT is set equal to 2.0, the normal output data is produced plus a Versatec plotting subroutine (VERTEC) is called. The subroutine outputs, via the Versatec plotter, plots of C_p versus X/C for each wing section of the final mesh calculations. This routine is simply putting into plot form the C_p and X/C numerical data contained in the normal output. A sample of the Versatec plot is presented in Fig. 2.4.

SECTION CP DATA

* = UPPER SURFACE
 + = LOWER SURFACE



SPAN STATION = 2.550

MACH	0.800	YAW	0.000	AOA	2.000
CL	0.34675	CD	0.02234	CM	0.00123

Figure 2.4. Versatec Plot of Cp vs. X/C

III. INTERACTIVE INPUT PROGRAM FLO27IN

The input data file required for the FLO27 program is extensive. Errors in input data FORMAT will cause program errors at execution time. In order to eliminate these errors and reduce the input data workload, a computer terminal interactive program was written. This interactive program, called FLO27IN, is a user-friendly way of creating an input data file for the potential flow wing analysis program FLO27. The FLO27IN program source code is presented in Appendix F.

The interactive program, FLO27IN, when executed asks questions of the user in order to construct and write to the user's "A" disk the required FLO27 input data file. The following presents the step-by-step procedure for executing the interactive program FLO27IN.

STEP #1---Log on to any IBM 3033 interactive terminal
with your user number and password.

STEP #2---Once logged on and in the CMS operation mode
type:

CP LINK 0247P 191 120 RR then hit ENTER

STEP #3---The word PASSWORD will appear, Type and ENTER

AERO

STEP #4---Type and ENTER

ACC 120 D

STEP #5---Type and ENTER

LOAD FLO27IN (START

The screen will display the header for the interactive program. Answer each question presented. At the end of each question in parenthesis is the input data variable associated with that question and whether the input parameter is a real number (R) or an integer (I). Example:
==> Enter the free stream Mach number (FMACH): (R). FMACH is the input data variable for the question. As you proceed through the FLC27IN program, opportunities to review and change input data will be presented. Should it become necessary to change your input data after completing the FLO27IN program, you can simply XEDIT the created data file.

The FLO27IN program also incorporates a library which contains the wing-section defining data for a number of current wing shapes. A copy of this library is presented in Appendix B. This feature will be displayed during program execution by the use of a menu from which the user can select a pre-defined wing section or define his own.

Upon completion of user inputs to the interactive program three additional data lines are automatically written to the bottom of the input file. They are:

END OF CALCULATION

FNX

0.0

In addition, Job Control Language (JCL) cards are written to the top and bottom of the file. All JCL cards start with a // format. After FLO27IN has run to completion type and enter RELEASE 191 to release the zero disk which was linked while executing the FLO27IN program. The created data file is written to the user's "A" disk with <filename> <filetype> of FLO27 DATAIN. Additional changes can be made simply by entering the XEDIT mode and editing the file.

IV. FLO27 BAICH SYSTEM EXECUTION

The potential flow program FLO27 can be executed after the input data file has been created. The batch processor is required for FLO27 execution because of the extensive CPU time needed to run the program. While in the XEDIT mode, a standard JOB card must be added to the top of the FLO27 DATAIN file prior to submission for job execution. The JOB card has the form:

```
//jobname JOB (nnnn,pppp),'ident',CLASS=J
```

jobname = may contain up to 8 alphanumeric characters,

the first of which must be alphabetic.

nnnn = your user number

pppp = project number, assigned by professor

'ident' = contains the user's own identification

information. A maximum of 20 characters may be contained within the single quotation marks.

After adding the JOB card to your data file, you are ready to execute the program. Type SUBMIT FLO27 DATAIN and press ENTER. Batch runs are normally not worth waiting for. To inquire about the status of the job, enter INQ and the job name used on the JOB card or "logoff". If the system is busy and the maximum mesh size was selected, it may be several hours before your job is run.

When the job is run the output will be spooled to the batch printer located next to the VM printer in the main computer building. The title at the top of the printout for batch jobs is the name entered on the JOB card. If it is desired to have the program output data spooled directly to the terminal, it will be necessary to add one additional JCL card to the input data set. This card must be placed immediately following the JOB card and has the form:

```
//*MAIN ORG=NPGVM1.nnnnP
```

where nnnn = your user number

Inserting this card in the input data will cause all program output to be spooled to the user's virtual reader where it may be looked at, printed or transferred to his "A" disk. To enquire as to whether information is in the reader simply type RDR and hit enter, then follow the instructions on the screen.

V. PROGFAM TEST RESULTS

The FLO27 program was tested in three stages; (1) during the reprogramming phase for conversion completeness, (2) after successful conversion with suitable wing data for program accuracy and (3) during an AE-4501 class project.

A. ACCEPTANCE TEST DATA

To test and ensure that the FLO27 program was converted to IEM compatible Fortran without error, an acceptance test data set was used. The acceptance test input and output data was supplied with the original CDC program source code. After conversion of the FLO27 program to Fortran suitable for the NPS IBM system, the acceptance test input data were run and the output results compared to the output generated by the CDC system.

Both output data sets were numerically exact when the FLO27 program was run in double precision on the IBM system. If the program was run in single precision, the numerical output values were exact to the third decimal place. The difference in single precision accuracy occurs because the CDC system uses a 64 bit word length while the IBM system word length in single precision is only 32 bits. It was

decided that the IBM single precision accuracy was satisfactory.

B. COMPARISON WITH OTHER PROGRAMS

The FLC27 program was also tested for accuracy by using the wing planform and section data from a NACA 572 wing. The data were run on both the FLO27 program and the Douglas potential flow program [Ref. 1]. The data generated by both programs was compared to wind tunnel data for the NACA 572 wing [Ref. 8]. The results are presented in Fig. 5.1 as plots of lift coefficient versus angle-of-attack. The results show that for the NACA 572 wing the FLO27 program more accurately predicts the wing lift coefficient than does the Douglas program.

C. AE-4501 CLASS PROJECT

The final test phase was conducted by introducing the FLO27 program into the AE-4501 course as a class project. This was accomplished to determine student problems/comments concerning the data input program FLO27IN and to test an additional wing shape. The wing chosen for study was that of the A-7 airplane. The A-7 wing has a distinct leading edge notch at the approximate mid-span. When the planform geometry was run with the notch included the FLO27 program

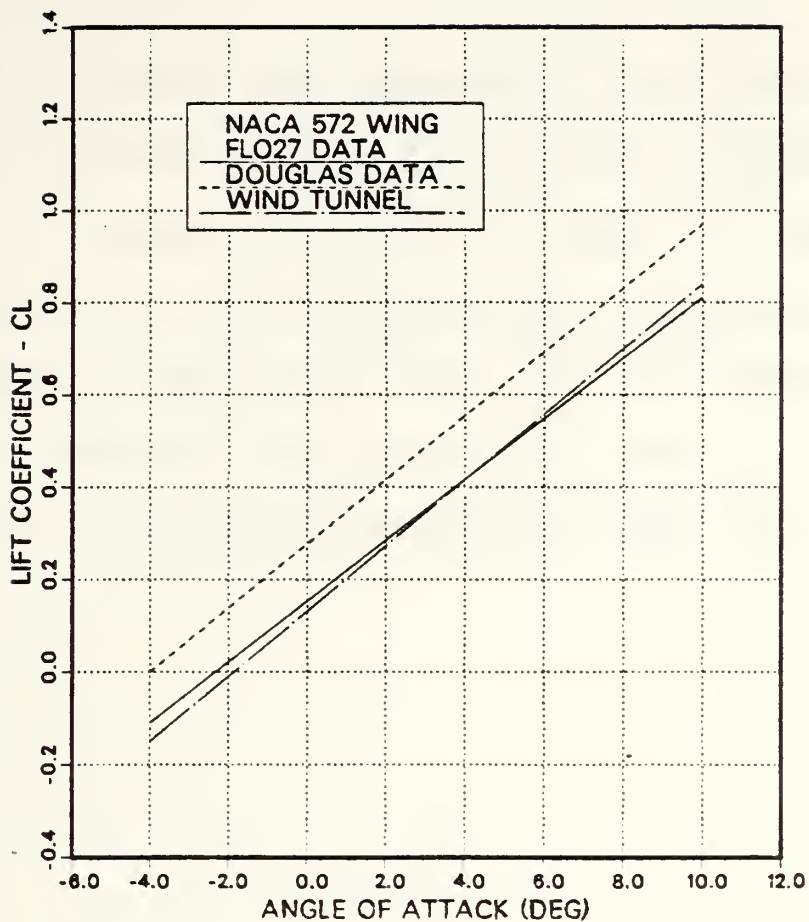


Figure 5.1. Program Calculated and Wind Tunnel Data

ran to completion but gave negative values for section and total induced drag coefficient. The value for the lift coefficient was low for the freestream Mach and angle-of-attack used. It was found that if the notch was

excluded from the wing geometry input data the program results were satisfactory both for induced drag and lift coefficient.

From the AE-4501 class experience it was determined that sharp wing planform discontinuities cannot be handled by the program. If however, the changes in shape are gradual, such as a wing glove, the program output appears to be satisfactory. Such was the case with the acceptance test case data where the wing geometry was that of the F-8 supercritical wing which incorporates a wing glove.

APPENDIX A

```
C This JCL routine allocates sufficient space on the mass
C storage system to store the entire tape contents
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=A
//* MAIN ORG=NEGVM1.3266P
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4C,DISP=(NEW,CATLG),
// DSN=MSS.S3266.WFLOW.DATA,SPACE=(CYL,(16,4,2))
/*
//
```

```
C This JCL routine is used to transfer all tape files to
C a partitioned data set in the mass storage system
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=J
//* MAIN ORG=NPGVM1.3266P
//COPY PROC FILE=,MEM=
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VCL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(&FILE,BLP,,IN)
// DCB=(RECFM=F,BLKSIZE=&0,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),
// DSN=MSS.S3266.WFLOW.SOURCE(&MEM),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=6400)
// PEND
// EXEC COPY,FILE=1,MEM=FLO27
// EXEC COPY,FILE=2,MEM=A411IN
// EXEC COPY,FILE=3,MEM=VWIN
// EXEC COPY,FILE=4,MEM=A411A01
// EXEC COPY,FILE=5,MEM=INTERF
// EXEC COPY,FILE=6,MEM=A411PS
// EXEC COPY,FILE=7,MEM=A411P1
// EXEC COPY,FILE=8,MEM=A411P2
// EXEC COPY,FILE=9,MEM=COUPLE
// EXEC COPY,FILE=10,MEM=ITER
// EXEC COPY,FILE=11,MEM=DATAIN
// EXEC COPY,FILE=12,MEM=FINAL
// EXEC COPY,FILE=13,MEM=BOEB1
// EXEC COPY,FILE=14,MEM=CONTPLT
// EXEC COPY,FILE=15,MEM=CORDPLT
// EXEC COPY,FILE=16,MEM=STREPLT
//COPY2 PROC FILE=,MEM=,LRECL=80,BLK=6400
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VOL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(&FILE,BLP,,IN)
// DCB=(RECFM=F,BLKSIZE=&LRECL,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),DSN=MSS.S3266.WFLOW.DATA(&MEM),
// DCB=(RECFM=FB,LRECL=&LRECL,BLKSIZE=&BLK)
// PEND
// EXEC COPY2,FILE=17,LRECL=150,BLK=6000,MEM=OUTF27
// EXEC COPY2,FILE=18,LRECL=150,BLK=6000,MEM=OUTIFC
// EXEC COPY2,FILE=19,LRECL=150,BLK=6000,MEM=OUT411L
// EXEC COPY2,FILE=20,LRECL=150,BLK=6000,MEM=OUT411U
/*
//
```



```

C This JCL routine moves all source code files from mass
C storage to the MVS 004 disk which can be accessed by
C entering GET MVS then following the screen instructions
C to move source files to your disk. If you want to move
C the data files to MVS 004 then change the word SOURCE
C to DATA in the JCL program below.
//JACK JOB (3266,0178), 'FASCHALL-2759', CLASS=A
//*MAIN ORG=NPGVM1.3266P
// EXEC PGM=IEBCOPY
//SYSPRINT DD SYSOUT=A
//FROM DD DISP=SHR, DSN=MSS.S3266.WFLOW.SOURCE
//INTO DD UNIT=3350, VOL=SER=MVS004, DISP=(NEW,KEEP),
// SPACE=(CYL,(16,4,10),RLSE), DSN=S3266.SOURCE
//SYSUT3 DD UNIT=SYSDA, SPACE=(CYL,(2,2))
//SYSUT4 DD UNIT=SYSDA, SPACE=(CYL,(2,2))
//SYSIN DD *
COPY OUTDD=INTC, INDD=FFCM
/*
//

```


APPENDIX B

LIERARY OF AIRFOIL SECTION GEOMETRIES

- 0 = user input section coordinate data
- 1 = flat plate data
- 2 = symmetrical wing (11% thickness at 30% chord)
- 3 = supercritical wing (cambered, 12% thickness at 32% chord)
- 4 = NACA 24-30-0 (cambered, 12% thickness at 30% chord)
- 5 = F-14 wing (cambered, 9.5% thickness at 37% chord)
- 6 = A-7 wing (7 deg droop at 20% chord, 7% thickness at 43% chord)
- 7 = LISSAMAN 7769 Airfoil (cambered, 11% thickness at 30% chord)
- 8 = NACA 0010 (symmetrical, 10% thickness at 30% chord)
- 9 = NACA 0010-34 (symmetrical, 10% thickness at 40% chord)
- 10 = NACA 0010-35 (symmetrical, 10% thickness at 50% chord)
- 11 = NACA 0010-64 (symmetrical, 10% thickness at 40% chord)
- 12 = NACA 0010-66 (symmetrical, 10% thickness at 60% chord)
- 13 = NACA 16-009 (symmetrical, 9% thickness at 50% chord)
- 14 = NACA 63-010 (symmetrical, 10% thickness at 35% chord)
- 15 = NACA 63A010 (symmetrical, 10% thickness at 35% chord)
- 16 = NACA 64-010 (symmetrical, 10% thickness at 40% chord)
- 17 = NACA 64A010 (symmetrical, 10% thickness at 40% chord)
- 18 = NACA 65-010 (symmetrical, 10% thickness at 40% chord)
- 19 = NACA 65A010 (symmetrical, 10% thickness at 40% chord)
- 20 = NACA 66-010 (symmetrical, 10% thickness at 45% chord)

APPENDIX C

THIS APPENDIX PRESENTS A COMPLETE INPUT DATA SET INCLUDING THE JCL CARDS REQUIRED TO EXECUTE THE PROGRAM FLC27

// (STANDARD JOB CARD -- SEE MVS USER'S GUIDE NO. MVS-01)

// EXEC FLC27

// GO.SYSIN DD *

SAMPLE DATA (NACA 572 WING SECTION)

FNX 40.0 FNY C FFLPT 0.0

FIT 100.0 C COVC 001

20.0 C CCCC001

5.0 C CCG001

FMACH YA C CDO 0.010000

O.10 O.9 DIFED

ZSYM FNS 3.0 SWEEP

I.0 XL C.0 YL 0.0 32.3275

ZS 0.0 CHORD 8.6000

FN 41.0 FUS 0.0

XP(I) YP(I)

1.0000000 0.0013000

0.8000000 0.0376000

0.5000000 0.0736000

0.2500000 0.0768000

0.1000000 0.0563000

0.0300000 0.0250000

0.0050000 0.0070000

0.0025000 0.0030000

0.0010000 0.0010000

0.0005000 0.0005000

0.0002500 0.0002500

0.0001000 0.0001000

0.0000500 0.0000500

0.0000250 0.0000250

0.0000100 0.0000100

0.0000050 0.0000050

0.0000025 0.0000025

ZS 9.6875 XL 6.1307

ZS 19.3750 XL 12.2614

END OF CALCULATION

FNX 0.0

//

THICK 1.0000 AT 0.0 FSEC 1.0

0.9000000 0.0120000 0.0204000
 0.6000000 0.0515000 0.0642000
 0.3000000 0.0780000 0.0788000
 0.1500000 0.0726000 0.0661000
 0.0400000 0.0414000 0.0350000
 0.0100000 0.0220000 0.0128000
 0.0010000 0.0050000 0.0012000
 0.0005000 0.0025000 0.000268000
 0.0002500 0.0012500 0.000042000
 0.0001000 0.0006250 0.00000412000
 0.0000500 0.0003125 0.00000026000
 0.0000250 0.0001562 0.000000082000

THICK AT FSEC
 1.0000 AT 0.0 FSEC 0.0
 1.0000 AT 0.0 FSEC 0.0

APPENDIX D

THIS APPENDIX PRESENTS THE FLG27 OUTPUT DATA PRODUCED FROM THE INPUT DATA OF THE PREVIOUS APPENDIX.

A46C MODIFIED FROM FLG27 OF ANTCNY JAMESON CURRANT INSTALUTE THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME FUSELAGE RAL

0.0
 SWEEP LIHED
 32.3275 0.0

PROFILE AT Z = 0.0 X SING Y SING
 TE ANGLE 16.0833 TE SLOPE -0.0720 0.0024 -0.0000

NL = 21, XF(NL) = 0.0

(XP,YP)

1.00000	-0.00130	0.95000	-0.00400	0.90000	-0.00820
0.60000	-0.02600	0.50000	-0.03200	0.40000	-0.03580
0.20000	-0.04220	0.15000	-0.04200	0.10000	-0.03750
0.03000	-0.02270	0.02000	-0.01680	0.01000	-0.01200
0.03000	0.02900	0.00250	0.00500	0.00500	0.00700
0.20000	0.07260	0.04000	0.03500	0.05000	0.04140
0.60000	0.06420	0.25000	0.07680	0.30000	0.07880
1.00000	0.00130	0.70000	0.05150	0.80000	0.03760

SECTION DEFINITION AT Z = 0.0

X LE	0.0	CHORD	8.6000	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0
X LE	0.0	CHORD	6.4500	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0

SECTION DEFINITION AT Z = 9.68750

X LE	0.0	CHORD	6.1307	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0
X LE	0.0	CHORD	4.3000	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0

SECTION DEFINITION AT Z = 19.37500

X LE	0.0	CHORD	4.3000	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0
X LE	0.0	CHORD	4.3000	THICKNESS RATIO	1.0000	TWIST	0.0
Y MIN	10	Y MAX	7880E-01	J MAX	33	Y DIF	0.0

ITERATIVE SOLUTION
 MACH NO
 0.10000
 NX
 40

NY

RELAX FCT 1
 1.60000
 ITERATION

RELAX FCT 2

RELAX FCT 3
 1.0000

ANG CF ATTACK
 2.0000
 NZ

ITERATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40						
J	5	4	4	4	4	4	4	4	4	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2					
I	31	21	21	21	21	21	21	21	21	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22				
MAX	0.6489	0.3389	0.2119	0.1356	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257	0.1257			
RELAX FCT 1	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000	1.60000		
RELAX FCT 2	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000			
RELAX FCT 3	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000			
ANG CF ATTACK	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000	2.0000			
MAX RESIDUAL	0.8247	0.1622	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433		
AVG CRRREC	0.3268	0.4054	0.4267	0.3269	0.2785	0.2040	0.1757	0.1389	0.1139	0.0876	0.0613	0.0543	0.0382	0.0273	0.0218	0.0161	0.0133	0.0109	0.0098	0.0087	0.0078	0.0070	0.0065	0.0060	0.0057	0.0055	0.0054	0.0053	0.0052	0.0051	0.0050	0.0049	0.0048	0.0047	0.0046	0.0045	0.0044	0.0043	0.0042	0.0041	0.0040	0.0039	0.0038	0.0037	0.0036	
MAX RESIDUAL	0.8247	0.1622	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433	0.2433

SECTION CHARACTERISTICS

MACH NO
 0.10000
 CL
 20238
 24033
 26515
 28127
 28695
 24168

SPAN STATION

0.0 7499
 3.8 7499
 7.7 4599
 11.6 2498
 15.4 9998
 19.3 7497

WING CHARACTERISTICS

MACH NO
 0.10000
 CL
 0.25575
 CM YAW
 -0.00467
 CD FCRM
 -0.32534E-02
 CM ROLL
 0.23919

ANG OF ATTACK

2.0000
 CD
 71088E-02
 24623E-02
 48115E-02
 57074E-02
 65451E-02
 70588E-02

CM

91575E-01
 58798E-01
 10506
 10920
 10935
 86038E-01

ANG OF ATTACK

2.0000
 CD FRICTION
 10000E-01
 CM PITCH
 -0.33140

L/D FORM

67466E-02

L/D
 37.

ITERATIVE SOLUTION
 MACH NO
 G.10000
 NX
 80

ANG CF ATTACK
 2.0000
 NZ
 16

NY

RELAX FCT 1	RELAX FCT 2	RELAX FCT 3	MAX	CORRECN	AVG	CCRREC	MAX RESIDAL	ITERATION
1	6	4	0.144217E-02	0.700000	0.01466E-03	0.1466E-03	0.16464E-02	1
2	2	13	0.585330E-03	1.44217E-02	0.074633E-04	0.74633E-04	0.12200E-02	2
3	2	13	0.31494E-03	1.1748E-03	0.055295E-04	0.55295E-04	0.10263E-02	3
4	2	11	0.22584E-03	1.1748E-03	0.042176E-04	0.42176E-04	0.84328E-03	4
5	2	18	0.18484E-03	1.4915E-03	0.031679E-04	0.31679E-04	0.72685E-03	5
6	2	7	0.16431E-03	1.3681E-03	0.026309E-04	0.26309E-04	0.63685E-03	6
7	2	6	0.14915E-03	1.2681E-03	0.024610E-04	0.24610E-04	0.58517E-03	7
8	2	5	0.13681E-03	1.1748E-03	0.023100E-04	0.23100E-04	0.53634E-03	8
9	2	4	0.12681E-03	1.0838E-03	0.021811E-04	0.21811E-04	0.46433E-03	9
10	2	3	0.11748E-03	0.98990E-04	0.020622E-04	0.20622E-04	0.42648E-03	10
11	2	3	0.10838E-03	0.85136E-04	0.019553E-04	0.19553E-04	0.40392E-03	11
12	2	3	0.98990E-04	0.78993E-04	0.018529E-04	0.18529E-04	0.40392E-03	12
13	2	3	0.85136E-04	0.73568E-04	0.017596E-04	0.17596E-04	0.38479E-03	13
14	2	3	0.78993E-04	0.65470E-04	0.016727E-04	0.16727E-04	0.36746E-03	14
15	2	3	0.73568E-04	0.61961E-04	0.015917E-04	0.15917E-04	0.34705E-03	15
16	2	3	0.65470E-04	0.61961E-04	0.015159E-04	0.15159E-04	0.32833E-03	16
17	2	3	0.61961E-04	0.61961E-04	0.014450E-04	0.14450E-04	0.30978E-03	17
18	2	3	0.61961E-04	0.61961E-04	0.013783E-04	0.13783E-04	0.29637E-03	18
19	2	3	0.61961E-04	0.61961E-04	0.013137E-04	0.13137E-04	0.28720E-03	19
20	2	3	0.61961E-04	0.61961E-04	0.012487E-04	0.12487E-04	0.28720E-03	20
MAX RESIDAL 1	MAX RESIDAL 2	MAX RESIDAL 3	MAX	MAX	MAX	MAX	MAX	MAX
-0.1646E-C2	-0.2872E-03	-0.2872E-03	-0.1646E-C2	-0.2872E-03	-0.2872E-03	-0.2872E-03	-0.2872E-03	-0.2872E-03

WORK
 19.0000

J	I	MAX RESIDAL	CONV	TOLERANCE
8	2	0.16464E-02	0.9122	0.1000E-05
7	80	0.12200E-02		
7	80	0.10263E-02		
7	80	0.84328E-03		
7	80	0.72685E-03		
7	2	0.63685E-03		
7	2	0.58517E-03		
7	2	0.53634E-03		
7	2	0.46433E-03		
7	2	0.42648E-03		
7	2	0.40392E-03		
6	2	0.38479E-03		
6	2	0.36746E-03		
6	2	0.34705E-03		
6	2	0.32833E-03		
6	2	0.30978E-03		
6	2	0.29637E-03		
5	2	0.28720E-03		
5	2	0.28720E-03		

SECTION CHARACTERISTICS
MACH NO 0.10000
YAW 0
SPAN STATION CL
0.0 22093
1.93750 .24319
3.87499 .26053
5.81249 .27508
7.74995 .28683
9.68749 .29643
11.62499 .30359
13.56248 .30863
15.49998 .30746
17.43747 .29141
19.37497 .21866

WING CHARACTERISTICS
MACH NO 0.10000
YAW 0
CL 0
CD FGRM-03 .87151E-03
CM YAW CM RCLL .25615
-0.00145

ANG GF ATTACK 2.0000
CD 18197E-01
.53303E-02
.14154E-C2
.44517E-C3
.72064E-03
.11954E-02
.16262E-02
.20637E-02
.27385E-C2
.41055E-02
.42003E-02

ANG GF ATTACK 2.0000
CD FRICTICN .10000E-01
CM PITCH .35963

CM
.10566
.10667
.10952
.11248
.11524
.11750
.11920
.11986
.11812
.10990
.78297E-01

L/D FORM 317.42
L/D 25.


```

ITERATIVE SOLUTION
MACH NO YAW .0
G.1 C000
NX
160
RELAX FCT 1 RELAX FCT 2 RELAX FCT 3
1.2 0000 700000 1.0000
ITERATION 1 2 3 4 5
MAX CORRREC 0.95314E-03 0.96428E-03 0.42692E-03 0.24824E-03 0.21125E-03
MAX RESIDAL 1 MAX RESIDAL 2
-0.1385E-C2 MAX 0.6224E-03
ANG OF ATTACK
2.0000
NZ
32
RELAX FCT 3
1.0000
J 17 17 15 15
K 4 23 15 16
AVG CRRREC 0.20565E-04 0.12764E-04 0.96224E-05 0.79284E-05 0.71493E-05
RELUCTN/CYCLE CONV 0.6224E-03
TOLERANCE
WORK 4.000C
0.8187
MAX RESIDAL 1 2 160 160 160 160
-0.1385E-02 0.98673E-03 0.87373E-03 0.73407E-03 0.6224E-03
J 16 15 15 15
K 24 3 3 3

```


SECTION CHARACTERISTICS
MACH NO
0.1000
SPAN 0.0
STATION
0.0 6875
1.0 93750
2.0 90625
3.0 87499
4.0 84374
5.0 81249
6.0 78124
7.0 74999
8.0 71874
9.0 68749
10.0 65624
11.0 62499
12.0 59373
13.0 56248
14.0 53123
15.0 49998
16.0 46872
17.0 43747
18.0 40622
19.0 37497

ANG OF ATTACK
2.0000
CD
.25222E-01
.13934E-01
.81933E-02
.57553E-02
.42526E-02
.34296E-02
.28453E-02
.24550E-02
.21906E-02
.16846E-02
.14920E-02
.12848E-02
.10850E-03
.83827E-03
.58364E-03
.22256E-03
.30467E-03
.14655E-03
.49591E-03
.68273E-04

CM
.11051
.10917
.10974
.11099
.11244
.11393
.11546
.11686
.11821
.11944
.12056
.12147
.12229
.12276
.12287
.12235
.12093
.11776
.11177
.95299E-01
.76890E-01

WING CHARACTERISTICS
MACH NO
0.1000
CL
0.28117
CM YAW
0.00116
CD
.38318E-02
CM RCLL
.25975
FCRM
.0

ANG OF ATTACK
2.0000
CD FRICTION
.10000E-01
CM PITCH
-.36670

L/D FORM
73.379
L/D
20.

CD
.13832E-01

A46C MODIFIED FROM FLC27 OF ANTCNY JAMESON, CURRANT INST ILUTE
THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME
BOEING VERSION, PREPARED BY DR. HAI-CHOW CHEN STANDARD BOEING INPUT FORMAT
END OF CALCULATION

SPAN NO. STATION DATA = PCINTS = 0.0

SPAN NO.	X/C	CP	CP	X/C	CP	CP	X/C	CP	X/C	CP	CP	X/C	CP	X/C	CP
1	0.846	0.000	1.955	0.560	0.492	1.955	0.560	0.492	0.774	0.777	1.430	0.883	0.857	0.101	0.585
0	0.706	0.152	0.787	0.810	0.396	0.557	0.810	0.396	0.740	0.105	0.348	0.740	0.105	0.000	0.716
0	0.578	0.298	0.072	0.548	0.303	0.572	0.548	0.303	0.609	0.077	0.085	0.609	0.077	0.000	0.434
0	0.360	0.542	0.038	0.336	0.287	0.178	0.336	0.287	0.385	0.031	0.245	0.385	0.031	0.000	0.180
0	0.270	0.525	0.060	0.255	0.226	0.140	0.255	0.226	0.291	0.041	0.183	0.291	0.041	0.000	0.458
0	0.193	0.235	0.117	0.172	0.332	0.140	0.172	0.332	0.143	0.058	0.153	0.143	0.058	0.000	0.672
0	0.128	0.543	0.133	0.108	0.441	0.375	0.108	0.441	0.188	0.011	0.209	0.188	0.011	0.000	0.183
0	0.078	0.058	0.124	0.065	0.385	0.155	0.065	0.385	0.048	0.036	0.255	0.048	0.036	0.000	0.766
0	0.038	0.378	0.019	0.030	0.185	0.079	0.030	0.185	0.024	0.013	0.243	0.024	0.013	0.000	0.299
0	0.001	0.527	0.077	0.003	0.665	0.335	0.003	0.665	0.066	0.018	0.644	0.066	0.018	0.000	0.343
0	0.001	0.527	0.416	0.003	0.955	0.821	0.003	0.955	0.066	0.187	0.378	0.066	0.187	0.000	0.067
0	0.012	0.560	0.232	0.015	0.419	0.582	0.015	0.419	0.222	0.008	0.130	0.222	0.008	0.000	0.828
0	0.035	0.675	0.667	0.043	0.319	0.280	0.043	0.319	0.522	0.058	0.169	0.522	0.058	0.000	0.768
0	0.072	0.512	0.109	0.052	0.263	0.152	0.052	0.263	0.969	0.124	0.202	0.969	0.124	0.000	0.804
0	0.124	0.444	0.265	0.092	0.350	0.475	0.092	0.350	0.550	0.137	0.259	0.550	0.137	0.000	0.429
0	0.188	0.945	0.354	0.101	0.521	0.669	0.101	0.521	0.266	0.134	0.382	0.266	0.134	0.000	0.440
0	0.357	0.204	0.394	0.288	0.169	0.475	0.288	0.169	0.407	0.171	0.335	0.407	0.171	0.000	0.587
0	0.460	0.617	0.330	0.488	0.449	0.583	0.488	0.449	0.517	0.071	0.335	0.517	0.071	0.000	0.451
0	0.576	0.692	0.330	0.607	0.694	0.928	0.607	0.694	0.639	0.486	0.806	0.639	0.486	0.000	0.451
0	0.705	0.351	0.224	0.733	0.502	0.389	0.733	0.502	0.774	0.388	0.862	0.774	0.388	0.000	0.155
0	0.846	0.000	0.091	0.883	0.370	0.350	0.883	0.370	0.521	0.112	0.262	0.521	0.112	0.000	0.223
1	0.000	0.000	0.211	0.000	0.000	0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.575

SPAN NO. STATION DATA = PCINTS = 0.96875

SPAN NO.	X/C	CP	CP	X/C	CP	CP	X/C	CP	X/C	CP	CP	X/C	CP	X/C	CP
1	0.846	0.000	2.356	0.560	0.492	2.042	0.560	0.492	0.521	0.777	1.559	0.883	0.857	0.101	0.670
0	0.706	0.152	0.094	0.810	0.396	0.485	0.810	0.396	0.740	0.166	0.486	0.740	0.166	0.000	0.556
0	0.578	0.298	0.081	0.548	0.303	0.485	0.548	0.303	0.609	0.053	0.244	0.609	0.053	0.000	0.280
0	0.463	0.542	0.031	0.336	0.287	0.166	0.336	0.287	0.385	0.015	0.183	0.385	0.015	0.000	0.515
0	0.360	0.525	0.052	0.255	0.226	0.133	0.255	0.226	0.291	0.031	0.139	0.291	0.031	0.000	0.839
0	0.270	0.525	0.114	0.172	0.332	0.164	0.172	0.332	0.159	0.022	0.133	0.159	0.022	0.000	0.173
0	0.193	0.235	0.177	0.108	0.441	0.336	0.108	0.441	0.143	0.051	0.209	0.143	0.051	0.000	0.487
0	0.128	0.543	0.133	0.065	0.385	0.155	0.065	0.385	0.048	0.036	0.255	0.048	0.036	0.000	0.487
0	0.078	0.058	0.124	0.030	0.185	0.079	0.030	0.185	0.024	0.013	0.243	0.024	0.013	0.000	0.370
0	0.038	0.378	0.019	0.003	0.665	0.335	0.003	0.665	0.066	0.018	0.644	0.066	0.018	0.000	0.492
0	0.001	0.527	0.077	0.003	0.955	0.821	0.003	0.955	0.066	0.187	0.378	0.066	0.187	0.000	0.476
0	0.001	0.527	0.416	0.003	0.955	0.821	0.003	0.955	0.066	0.187	0.378	0.066	0.187	0.000	0.547
0	0.012	0.560	0.232	0.015	0.419	0.582	0.015	0.419	0.222	0.008	0.130	0.222	0.008	0.000	0.147
0	0.035	0.675	0.667	0.043	0.319	0.280	0.043	0.319	0.522	0.058	0.169	0.522	0.058	0.000	0.333
0	0.072	0.512	0.109	0.052	0.263	0.152	0.052	0.263	0.969	0.124	0.202	0.969	0.124	0.000	0.429
0	0.124	0.444	0.265	0.092	0.350	0.475	0.092	0.350	0.266	0.134	0.382	0.266	0.134	0.000	0.440
0	0.188	0.945	0.354	0.101	0.521	0.669	0.101	0.521	0.407	0.171	0.335	0.407	0.171	0.000	0.587
0	0.357	0.204	0.394	0.288	0.169	0.475	0.288	0.169	0.517	0.071	0.335	0.517	0.071	0.000	0.451
0	0.460	0.617	0.330	0.488	0.449	0.583	0.488	0.449	0.639	0.486	0.806	0.639	0.486	0.000	0.451
0	0.576	0.692	0.330	0.607	0.694	0.928	0.607	0.694	0.639	0.486	0.806	0.639	0.486	0.000	0.155
0	0.705	0.351	0.224	0.733	0.502	0.389	0.733	0.502	0.774	0.388	0.862	0.774	0.388	0.000	0.223
0	0.846	0.000	0.091	0.883	0.370	0.350	0.883	0.370	0.521	0.112	0.262	0.521	0.112	0.000	0.575
1	0.000	0.000	0.211	0.000	0.000	0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.147

SPAN STATION = 4.84374
 NO. CF DATA PCINTS = 101

0.460617	-0.372240	0.488449	-0.356717	0.517071	-0.341032	0.546485	-0.322554
0.576692	-0.301548	0.607694	-0.272598	0.639466	-0.237831	0.672056	-0.202293
0.705355	-0.173943	0.739502	-0.150774	0.774388	-0.124863	0.810059	-0.096446
0.846511	-0.036027	0.883730	0.014850	0.921712	0.068256	0.960470	0.146866
1.000000	-0.217029						

1.000000	0.84374	0.960492	0.208446	0.521777	0.163078	0.883857	0.130665
0.846730	0.810258	0.810258	0.083923	0.774854	0.063487	0.740105	0.045366
0.706152	0.672558	0.672558	0.030518	0.640641	0.032970	0.609077	0.022422
0.578298	0.548303	0.548303	0.006677	0.519059	0.009567	0.490615	0.002653
0.463050	0.436282	0.436282	0.001760	0.413941	0.001524	0.391838	0.001081
0.360542	0.350026	0.350026	0.001173	0.330321	0.001924	0.311358	0.001193
0.270527	0.275143	0.275143	0.001651	0.259222	0.001972	0.243458	0.001754
0.193235	0.188053	0.188053	0.001660	0.159106	0.001586	0.148531	0.001410
0.128548	0.120671	0.120671	0.002296	0.101507	0.001591	0.088533	0.001754
0.080050	0.093055	0.093055	0.005722	0.055514	0.003305	0.046634	0.002275
0.038078	0.061988	0.061988	0.024930	0.024315	0.006301	0.003556	0.005461
0.013378	0.041359	0.041359	0.035401	0.009184	0.014551	0.003622	0.005613
0.001528	0.029509	0.029509	0.065640	0.003555	0.032597	0.000918	0.005191
0.002560	0.017411	0.017411	0.049209	0.001704	0.022008	0.000617	0.004519
0.035734	0.155255	0.155255	0.329758	0.096572	0.509778	0.061694	0.108850
0.072512	0.613255	0.613255	0.586730	0.955014	0.459344	0.110347	0.473355
0.188946	0.481388	0.481388	0.507402	0.155512	0.524044	0.171564	0.517203
0.266567	0.510275	0.510275	0.457852	0.266132	0.519221	0.245938	0.519503
0.357205	0.445434	0.445434	0.426587	0.310273	0.480835	0.233338	0.444144
0.460618	0.374505	0.374505	0.435877	0.407327	0.440835	0.243357	0.435107
0.576692	0.301668	0.301668	0.358325	0.517072	0.342105	0.433485	0.322413
0.705355	0.172896	0.172896	0.272327	0.639466	0.237235	0.672056	0.208536
0.846511	0.034988	0.034988	0.149667	0.774388	0.063731	0.810059	0.044782
1.000000	0.217983	0.883730	0.016212	0.921712	0.068660	0.960470	0.14782

SPAN STATION = 5.81249
 NO. CF DATA PCINTS = 101

1.000000	5.81249	0.960492	0.208991	0.521777	0.163620	0.883857	0.13160
0.846730	0.810681	0.810681	0.085422	0.774854	0.064850	0.740105	0.04673
0.706152	0.674877	0.674877	0.032016	0.640642	0.034332	0.609077	0.02352
0.578298	0.548796	0.548796	0.008583	0.519059	0.007570	0.490693	0.00245
0.463090	0.436282	0.436282	0.001176	0.410261	0.001449	0.385015	0.00088
0.360542	0.350026	0.350026	0.000650	0.313940	0.000881	0.291851	0.000595
0.270527	0.275143	0.275143	0.001428	0.230322	0.001119	0.211358	0.000856
0.193235	0.188053	0.188053	0.001653	0.159225	0.001534	0.143458	0.001195
0.128548	0.120671	0.120671	0.002296	0.101106	0.001534	0.088501	0.001656
0.080050	0.093055	0.093055	0.005722	0.055119	0.003301	0.046634	0.002275
0.038078	0.061988	0.061988	0.024930	0.024315	0.006301	0.003556	0.005461
0.013378	0.041359	0.041359	0.035401	0.009184	0.014551	0.003622	0.005613
0.001528	0.029509	0.029509	0.065640	0.003555	0.032597	0.000918	0.005191
0.002560	0.017411	0.017411	0.049209	0.001704	0.022008	0.000617	0.004519
0.035734	0.155255	0.155255	0.329758	0.096572	0.509778	0.061694	0.108850
0.072512	0.613255	0.613255	0.586730	0.955014	0.459344	0.110347	0.473355
0.188946	0.481388	0.481388	0.507402	0.155512	0.524044	0.171564	0.517203
0.266567	0.510275	0.510275	0.457852	0.266132	0.519221	0.245938	0.519503
0.357205	0.445434	0.445434	0.426587	0.310273	0.480835	0.233338	0.444144
0.460618	0.374505	0.374505	0.435877	0.407327	0.440835	0.243357	0.435107
0.576692	0.301668	0.301668	0.358325	0.517072	0.342105	0.672056	0.322413
0.705355	0.172896	0.172896	0.272327	0.639466	0.237235	0.810059	0.208536
0.846511	0.034988	0.034988	0.149667	0.774388	0.063731	0.960470	0.044782
1.000000	0.217983	0.883730	0.016212	0.921712	0.068660	0.960470	0.14782

SPAN NO. 74959

SPAN NO.	CF	DATA	POINTS	FC	INTS	74959	IOI	X/C	CP	X/C	CP	X/C	CP	X/C	CP
1	0	000	000	0	0	000	0	0	0	0	0	0	0	0	0
1	0	846	1528	0	0	000	0	0	0	0	0	0	0	0	0
0	0	706	1298	0	0	000	0	0	0	0	0	0	0	0	0
0	0	578	298	0	0	000	0	0	0	0	0	0	0	0	0
0	0	463	0542	0	0	000	0	0	0	0	0	0	0	0	0
0	0	360	542	0	0	000	0	0	0	0	0	0	0	0	0
0	0	270	5235	0	0	000	0	0	0	0	0	0	0	0	0
0	0	193	2543	0	0	000	0	0	0	0	0	0	0	0	0
0	0	128	658	0	0	000	0	0	0	0	0	0	0	0	0
0	0	038	378	0	0	000	0	0	0	0	0	0	0	0	0
0	0	013	378	0	0	000	0	0	0	0	0	0	0	0	0
0	0	001	527	0	0	000	0	0	0	0	0	0	0	0	0
0	0	001	528	0	0	000	0	0	0	0	0	0	0	0	0
0	0	012	734	0	0	000	0	0	0	0	0	0	0	0	0
0	0	072	512	0	0	000	0	0	0	0	0	0	0	0	0
0	0	124	544	0	0	000	0	0	0	0	0	0	0	0	0
0	0	188	546	0	0	000	0	0	0	0	0	0	0	0	0
0	0	266	565	0	0	000	0	0	0	0	0	0	0	0	0
0	0	357	205	0	0	000	0	0	0	0	0	0	0	0	0
0	0	460	618	0	0	000	0	0	0	0	0	0	0	0	0
0	0	576	692	0	0	000	0	0	0	0	0	0	0	0	0
0	0	705	395	0	0	000	0	0	0	0	0	0	0	0	0
0	0	846	511	0	0	000	0	0	0	0	0	0	0	0	0
1	0	000	000	0	0	000	0	0	0	0	0	0	0	0	0

SPAN NO.	CF	DATA	POINTS	FC	INTS	871874	IOI	X/C	CP	X/C	CP	X/C	CP	X/C	CP
1	0	000	000	0	0	000	0	0	0	0	0	0	0	0	0
1	0	846	1528	0	0	000	0	0	0	0	0	0	0	0	0
0	0	706	1298	0	0	000	0	0	0	0	0	0	0	0	0
0	0	578	298	0	0	000	0	0	0	0	0	0	0	0	0
0	0	463	0542	0	0	000	0	0	0	0	0	0	0	0	0
0	0	360	542	0	0	000	0	0	0	0	0	0	0	0	0
0	0	270	5235	0	0	000	0	0	0	0	0	0	0	0	0
0	0	193	2542	0	0	000	0	0	0	0	0	0	0	0	0
0	0	128	658	0	0	000	0	0	0	0	0	0	0	0	0
0	0	038	378	0	0	000	0	0	0	0	0	0	0	0	0
0	0	013	378	0	0	000	0	0	0	0	0	0	0	0	0
0	0	001	527	0	0	000	0	0	0	0	0	0	0	0	0
0	0	001	528	0	0	000	0	0	0	0	0	0	0	0	0
0	0	012	734	0	0	000	0	0	0	0	0	0	0	0	0
0	0	072	512	0	0	000	0	0	0	0	0	0	0	0	0
0	0	124	544	0	0	000	0	0	0	0	0	0	0	0	0
0	0	188	546	0	0	000	0	0	0	0	0	0	0	0	0
0	0	266	565	0	0	000	0	0	0	0	0	0	0	0	0
0	0	357	205	0	0	000	0	0	0	0	0	0	0	0	0
0	0	460	618	0	0	000	0	0	0	0	0	0	0	0	0
0	0	576	692	0	0	000	0	0	0	0	0	0	0	0	0
0	0	705	395	0	0	000	0	0	0	0	0	0	0	0	0
0	0	846	511	0	0	000	0	0	0	0	0	0	0	0	0
1	0	000	000	0	0	000	0	0	0	0	0	0	0	0	0

SPAN STATION = 5.68749
 ND. X/C DATA POINTS = 101

0.0	0.357734	0.0	0.43503	0.0	0.82653	0.0	0.52901	0.0	0.61655	0.0	0.66571
0.0	0.072512	0.0	0.084320	0.0	0.360660	0.0	0.096972	0.0	0.110348	0.0	0.51149
0.0	0.124446	0.0	0.353137	0.0	0.535584	0.0	0.155014	0.0	0.171564	0.0	0.54018
0.0	0.188933	0.0	0.207131	0.0	0.547911	0.0	0.226274	0.0	0.245939	0.0	0.54082
0.0	0.266444	0.0	0.288015	0.0	0.548032	0.0	0.310277	0.0	0.333337	0.0	0.40171
0.0	0.357205	0.0	0.381869	0.0	0.440053	0.0	0.407321	0.0	0.433548	0.0	0.40332
0.0	0.460454	0.0	0.488449	0.0	0.366620	0.0	0.517011	0.0	0.546485	0.0	0.30332
0.0	0.383905	0.0	0.488449	0.0	0.275504	0.0	0.639486	0.0	0.672056	0.0	0.20861
0.0	0.570518	0.0	0.739542	0.0	0.215127	0.0	0.774388	0.0	0.810059	0.0	0.20861
0.0	0.705395	0.0	0.739542	0.0	0.151272	0.0	0.921712	0.0	0.960470	0.0	0.14453
0.0	0.846511	0.0	0.883730	0.0	0.016212	0.0	0.521712	0.0	0.0	0.0	0.0
1.0	0.000000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SPAN STATION = 5.68749
 ND. X/C DATA POINTS = 101

1.0	0.000000	0.0	0.560492	0.0	0.209400	0.0	0.527777	0.0	0.883857	0.0	0.1310
0.0	0.8406730	0.0	0.8102598	0.0	0.387738	0.0	0.774642	0.0	0.740105	0.0	0.1310
0.0	0.578297	0.0	0.548303	0.0	0.013896	0.0	0.519059	0.0	0.609077	0.0	0.0314
0.0	0.463090	0.0	0.436282	0.0	0.005305	0.0	0.410261	0.0	0.385015	0.0	0.01364
0.0	0.370542	0.0	0.350826	0.0	0.056556	0.0	0.330321	0.0	0.291831	0.0	0.05605
0.0	0.193235	0.0	0.175841	0.0	0.150804	0.0	0.259224	0.0	0.214357	0.0	0.14248
0.0	0.128422	0.0	0.114441	0.0	0.142402	0.0	0.101106	0.0	0.088501	0.0	0.14248
0.0	0.076658	0.0	0.065635	0.0	0.153562	0.0	0.55507	0.0	0.046626	0.0	0.12243
0.0	0.038057	0.0	0.030918	0.0	0.372567	0.0	0.55507	0.0	0.018659	0.0	0.51337
0.0	0.013377	0.0	0.003625	0.0	0.640405	0.0	0.024312	0.0	0.003362	0.0	0.51337
0.0	0.015228	0.0	0.003625	0.0	0.400627	0.0	0.06186	0.0	0.009017	0.0	0.27006
0.0	0.012560	0.0	0.017041	0.0	0.392173	0.0	0.022008	0.0	0.028618	0.0	0.17706
0.0	0.032734	0.0	0.043503	0.0	0.614254	0.0	0.096972	0.0	0.061654	0.0	0.51506
0.0	0.072512	0.0	0.084319	0.0	0.545503	0.0	0.155014	0.0	0.171564	0.0	0.54552
0.0	0.124446	0.0	0.139315	0.0	0.552637	0.0	0.220131	0.0	0.245939	0.0	0.54552
0.0	0.188933	0.0	0.207137	0.0	0.442727	0.0	0.310277	0.0	0.333337	0.0	0.40337
0.0	0.266444	0.0	0.288168	0.0	0.427727	0.0	0.407321	0.0	0.433351	0.0	0.30337
0.0	0.357205	0.0	0.381868	0.0	0.368527	0.0	0.517011	0.0	0.546485	0.0	0.20573
0.0	0.460454	0.0	0.488450	0.0	0.277915	0.0	0.639486	0.0	0.672056	0.0	0.20573
0.0	0.570518	0.0	0.607694	0.0	0.215166	0.0	0.774388	0.0	0.810059	0.0	0.14452
0.0	0.705395	0.0	0.739502	0.0	0.151212	0.0	0.921712	0.0	0.960470	0.0	0.14452
0.0	0.846511	0.0	0.883733	0.0	0.016212	0.0	0.521712	0.0	0.0	0.0	0.0
1.0	0.000000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SPAN STATION = 10.65624
 ND. X/C DATA POINTS = 101

1.0	0.000000	0.0	0.960492	0.0	0.209400	0.0	0.527777	0.0	0.883857	0.0	0.1310
0.0	0.846730	0.0	0.810396	0.0	0.387738	0.0	0.774854	0.0	0.740105	0.0	0.0313
0.0	0.706152	0.0	0.672558	0.0	0.013896	0.0	0.521777	0.0	0.609907	0.0	0.03869

SPAN NO.	STATION	DATA	POLY	POINTS	11.62	499
0	578	298	030	109	0	548
0	460	090	008	784	0	436
0	360	542	031	054	0	336
0	270	235	011	852	0	250
0	198	658	016	167	0	144
0	038	050	044	282	0	060
0	013	378	031	539	0	009
0	001	527	064	224	0	003
0	001	528	042	152	0	003
0	012	560	021	681	0	017
0	035	734	068	402	0	043
0	072	444	264	253	0	084
0	188	546	051	180	0	135
0	266	567	053	369	0	207
0	357	205	053	573	0	280
0	460	618	046	785	0	381
0	576	692	030	561	0	487
0	705	395	017	649	0	607
0	846	511	035	703	0	739
1	000	000	022	043	0	883

SPAN NO.	STATION	DATA	POLY	POINTS	11.62	499
0	490	654	000	107	0	519
0	385	015	000	345	0	410
0	291	831	007	782	0	313
0	143	458	009	829	0	230
0	086	501	017	291	0	159
0	046	334	031	095	0	055
0	008	556	018	178	0	024
0	000	363	063	272	0	006
0	009	017	020	084	0	061
0	009	618	033	269	0	064
0	028	618	095	793	0	022
0	061	694	070	009	0	052
0	171	564	056	663	0	096
0	245	939	055	325	0	155
0	333	338	050	682	0	226
0	546	485	032	506	0	407
0	672	056	034	260	0	519
0	810	059	044	274	0	639
0	560	471	025	618	0	774

SPAN STATION DATA = 12.59373
 NO. OF DATA PCINTS = 101

0.460617	-0.385346	0.488450	-0.371584	0.517071	-0.353830	0.546485	-0.334443
0.576692	-0.310566	0.607694	-0.279852	0.639486	-0.243425	0.672056	-0.220707
0.705355	-0.176945	0.739502	-0.152886	0.774388	-0.126234	0.810059	-0.098703
0.846511	-0.035729	0.883730	0.016212	0.921712	0.0695618	0.960470	0.14572
1.000000	-0.220435						

1.000000	0.237601	0.560491	0.209400	0.521777	0.165122	0.883857	0.13351
0.846730	0.105264	0.810396	0.088283	0.774854	0.068256	0.740105	0.03354
0.706151	0.035646	0.672957	0.037193	0.640641	0.0039646	0.609077	0.003564
0.578298	0.003063	0.548303	0.005262	0.519059	0.001848	0.490653	0.001055
0.463050	0.000993	0.436848	0.002622	0.413940	0.000752	0.391831	0.000512
0.360542	0.000920	0.350026	0.001776	0.330321	0.000947	0.211358	0.000512
0.270527	0.004262	0.175832	0.014300	0.159222	0.016224	0.088501	0.001350
0.193233	0.015594	0.114441	0.032067	0.105106	0.012235	0.046334	0.001699
0.128543	0.031608	0.065635	0.017784	0.051507	0.019182	0.018626	0.002814
0.076658	0.053258	0.030635	0.037302	0.024313	0.050136	0.003555	0.005359
0.038050	0.083268	0.009184	0.063508	0.006189	0.061076	0.000917	0.004185
0.013378	0.140844	0.003262	0.070161	0.00166	0.031520	0.000901	0.002185
0.001528	0.240813	0.001704	0.031582	0.006159	0.010592	0.002861	0.002185
0.001256	0.392098	0.004350	0.045070	0.022308	0.059185	0.006165	0.007002
0.035734	0.658209	0.084320	0.415023	0.096972	0.566483	0.061654	0.053385
0.072512	0.938341	0.139315	0.559475	0.156014	0.576198	0.171564	0.578295
0.124445	0.571033	0.207137	0.363775	0.226131	0.515533	0.245938	0.557497
0.188944	0.545323	0.288014	0.530192	0.310273	0.512827	0.333338	0.54113
0.266567	0.465932	0.381868	0.472514	0.407326	0.428276	0.433576	0.43891
0.357204	0.390444	0.488449	0.372514	0.517071	0.354631	0.546485	0.33508
0.476652	0.311102	0.607694	0.280244	0.639486	0.243723	0.672056	0.20725
0.576355	0.177034	0.739502	0.152920	0.774388	0.0695618	0.810059	0.002869
0.705355	0.035524	0.883730	0.016212	0.921712	0.0695618	0.960470	0.001502
0.846511	0.220435						
1.000000	0.220435						

SPAN STATION DATA = 13.56248
 NO. OF DATA POINTS = 101

1.000000	0.237601	0.960492	0.209400	0.921777	0.165122	0.883857	0.13351
0.846730	0.109264	0.810396	0.088283	0.774854	0.068256	0.740105	0.03354
0.706152	0.039646	0.672958	0.037193	0.640642	0.0039646	0.609077	0.003564
0.578298	0.003063	0.548303	0.005262	0.519059	0.001848	0.490654	0.001055
0.463050	0.000993	0.436848	0.002622	0.413940	0.000752	0.391831	0.000512
0.360542	0.000920	0.350026	0.001776	0.330321	0.000947	0.291831	0.000512
0.270527	0.004262	0.175832	0.014300	0.230321	0.016224	0.211358	0.001350
0.193233	0.015594	0.114441	0.032067	0.159222	0.012235	0.088501	0.001699
0.128543	0.031608	0.065635	0.017784	0.105106	0.019182	0.046334	0.002814
0.076658	0.053258	0.030635	0.037302	0.024313	0.050136	0.003555	0.005359
0.038050	0.083268	0.009184	0.063508	0.006189	0.061076	0.000917	0.004185
0.013378	0.140844	0.003262	0.070161	0.00166	0.031520	0.000901	0.002185
0.001528	0.240813	0.001704	0.031582	0.006159	0.010592	0.002861	0.002185
0.001256	0.392098	0.004350	0.045070	0.022308	0.059185	0.006165	0.007002
0.035734	0.658209	0.084320	0.415023	0.096972	0.566483	0.061654	0.053385
0.072512	0.938341	0.139315	0.559475	0.156014	0.576198	0.171564	0.578295
0.124445	0.571033	0.207137	0.363775	0.226131	0.515533	0.245938	0.557497
0.188944	0.545323	0.288014	0.530192	0.310273	0.512827	0.333338	0.54113
0.266567	0.465932	0.381868	0.472514	0.407326	0.428276	0.433576	0.43891
0.357204	0.390444	0.488449	0.372514	0.517071	0.354631	0.546485	0.33508
0.476652	0.311102	0.607694	0.280244	0.639486	0.243723	0.672056	0.20725
0.576355	0.177034	0.739502	0.152920	0.774388	0.0695618	0.810059	0.002869
0.705355	0.035524	0.883730	0.016212	0.921712	0.0695618	0.960470	0.001502
0.846510	0.220435						
1.000000	0.220435						

SPAN OF DATA = 15.49998
 NO. OF DATA PCINTS = 101

SPAN NO.	OF DATA	PCINTS	CP	X/C	CP	X/C	CP	X/C	CP	X/C	CP	X/C	CP	X/C
1	0.00	0.00	2.2381	0.560	0.492	2.094	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.846	730	1.083	0.810	0.396	0.873	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.706	152	0.386	0.672	0.598	0.358	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.578	297	0.301	0.548	0.303	0.148	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.463	090	0.080	0.436	0.282	0.025	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.360	542	0.097	0.352	0.687	0.056	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.270	527	0.125	0.250	0.231	0.140	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.193	235	0.152	0.144	0.440	0.128	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.128	543	0.154	0.146	0.374	0.176	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.076	658	0.154	0.146	0.374	0.176	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.038	378	0.022	0.079	0.440	0.040	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.015	227	0.033	0.065	0.184	0.030	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.001	528	0.052	0.044	0.362	0.073	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.001	528	0.052	0.044	0.362	0.073	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.012	734	0.038	0.139	0.595	0.309	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.035	560	0.076	0.281	0.641	0.428	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.072	712	0.115	0.436	0.19	0.647	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.124	444	0.155	0.561	0.15	0.567	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.188	545	0.171	0.337	0.15	0.531	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.266	567	0.254	0.693	0.27	0.468	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.357	604	0.387	0.714	0.13	0.387	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.460	617	0.306	0.622	0.19	0.306	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.576	692	0.171	0.161	0.9	0.171	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.705	395	0.030	0.081	0.6	0.030	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.846	511	0.033	0.081	0.6	0.033	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.223	0.296	0.730	0.223	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

SPAN OF DATA = 16.46472
 NO. OF DATA PCINTS = 101

SPAN NO.	OF DATA	PCINTS	CP	X/C	CP	X/C	CP	X/C	CP	X/C	CP	X/C	CP	X/C
1	0.00	0.00	2.371	0.560	0.491	2.080	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.846	730	1.068	0.810	0.396	0.858	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.706	152	0.371	0.672	0.598	0.348	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.578	298	0.291	0.555	0.303	0.133	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.463	090	0.090	0.436	0.282	0.042	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.360	542	0.030	0.316	0.47	0.053	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.270	527	0.098	0.249	0.26	0.097	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.193	235	0.132	0.144	0.331	0.141	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.128	543	0.152	0.146	0.441	0.170	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.076	658	0.154	0.146	0.374	0.172	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.038	378	0.021	0.079	0.462	0.040	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.015	227	0.033	0.065	0.185	0.030	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.001	528	0.052	0.044	0.362	0.073	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.001	528	0.052	0.044	0.362	0.073	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.012	734	0.038	0.139	0.595	0.309	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.035	560	0.076	0.281	0.641	0.428	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.072	712	0.115	0.436	0.19	0.647	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.124	444	0.155	0.561	0.15	0.567	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.188	545	0.171	0.337	0.15	0.531	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.266	567	0.254	0.693	0.27	0.468	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.357	604	0.387	0.714	0.13	0.387	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.460	617	0.306	0.622	0.19	0.306	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.576	692	0.171	0.161	0.9	0.171	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.705	395	0.030	0.081	0.6	0.030	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0	0.846	511	0.033	0.081	0.6	0.033	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.077	0.244	0.8	0.077	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

0.578299	0.020027	0.548304	0.005313	0.519100	0.008821	0.490655	0.001611
0.463090	0.014509	0.436283	0.009060	0.410261	0.007357	0.385016	0.001502
0.360543	0.009728	0.336848	0.005458	0.313941	0.007597	0.291332	0.001502
0.270527	0.011074	0.250026	0.009629	0.239224	0.016191	0.213458	0.001547
0.198543	0.014752	0.175832	0.013802	0.159101	0.011347	0.143451	0.001245
0.076658	0.014735	0.065638	0.016066	0.055507	0.014748	0.046334	0.001456
0.038050	0.008437	0.030635	0.004976	0.024313	0.005577	0.018626	0.001545
0.001527	0.003333	0.009184	0.003896	0.006118	0.005170	0.003562	0.001450
0.001528	0.003660	0.003595	0.004344	0.006187	0.003020	0.009017	0.001484
0.012560	0.009727	0.017040	0.004542	0.022359	0.005966	0.028618	0.001763
0.032734	0.025705	0.043503	0.008491	0.096008	0.005541	0.061647	0.001617
0.072512	0.062254	0.130319	0.006136	0.096914	0.005351	0.110347	0.001566
0.124444	0.150391	0.34316	0.005290	0.156014	0.005361	0.171564	0.001503
0.188946	0.226718	0.207138	0.005173	0.226132	0.005110	0.245939	0.001503
0.266567	0.492530	0.381015	0.004759	0.310737	0.004583	0.333333	0.001437
0.357205	0.412362	0.281869	0.003906	0.401732	0.003699	0.433577	0.001352
0.460619	0.325703	0.487659	0.002149	0.517017	0.001943	0.546486	0.001116
0.576693	0.134664	0.607695	0.001145	0.639487	0.001936	0.672057	0.001116
0.705356	0.010874	0.739504	0.001145	0.774389	0.001919	0.810061	0.001570
0.846512	0.010874	0.883731	0.001145	0.921714	0.001919	0.960473	0.001544
1.000000	0.021893	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

SPAN ST ATIDA = 19.37497
 NO. CF DATA FCINTS = 101

1.000000	0.155040	0.960490	0.140190	0.521719	0.105858	0.883856	0.08106
0.846732	0.061987	0.810397	0.145366	0.774855	0.029564	0.740106	0.01580
0.706153	0.006267	0.672999	0.002861	0.640643	0.020340	0.609078	0.00245
0.463259	0.003576	0.548305	0.004748	0.519100	0.022857	0.490654	0.003445
0.360527	0.004705	0.436283	0.002066	0.410261	0.007517	0.385016	0.005058
0.270527	0.005793	0.336849	0.005855	0.239224	0.009490	0.213459	0.005644
0.198543	0.010842	0.175832	0.012780	0.159101	0.011307	0.143451	0.011279
0.076658	0.013504	0.065638	0.014105	0.055507	0.012102	0.046334	0.011250
0.038050	0.009747	0.030635	0.007724	0.024313	0.005871	0.018626	0.002179
0.001527	0.003374	0.009184	0.003283	0.006118	0.004208	0.003562	0.002177
0.001528	0.003640	0.003595	0.002231	0.006187	0.002081	0.009017	0.002177
0.012560	0.009746	0.017040	0.002035	0.022359	0.004269	0.028618	0.002177
0.032734	0.023528	0.043503	0.003571	0.096008	0.003695	0.061647	0.002177
0.072512	0.055985	0.130319	0.004084	0.156014	0.004609	0.110347	0.002178
0.124444	0.120119	0.34316	0.004084	0.226132	0.004403	0.245939	0.002178
0.188946	0.242211	0.487659	0.004084	0.310737	0.004396	0.333333	0.002178
0.266567	0.396456	0.607695	0.003847	0.401732	0.004123	0.433577	0.002178
0.357205	0.542211	0.739504	0.003847	0.517017	0.004396	0.546486	0.002178
0.460619	0.722110	0.883731	0.003847	0.639487	0.004396	0.672057	0.002178
0.576693	0.962211	0.960473	0.002866	0.774389	0.003333	0.810061	0.002178
0.705356	0.300170	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
0.846512	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

0.460619	-C.245829	0.488450	-0.239440	0.517072	-0.229495	0.546486	-0.21668
0.576693	-C.204904	0.607655	-0.186239	0.639487	-0.163666	0.672057	-0.14166
0.705356	-C.124829	0.739503	-0.112534	0.774389	-0.097547	0.810060	-0.07234
0.846512	-C.038530	0.883731	-0.006437	0.921712	0.025749	0.960469	0.07570
1.000000	-C.142642						

APPENDIX E

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE POTENTIAL FLOW PROGRAM FLO27.

```
*****9/12/83*****
THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING
FINITE VOLUME SCHEME WITH SHEARED PARABOLIC COORDINATES
PROGRAMMED BY ANTONY JAMESON, JANUARY-APRIL 1977
*****
THE BEING VERSION OF FLO27 WAS PREPARED BY CR. HAI-CHOW
CHEN WITH THE FOLLOWING MODIFICATIONS
1) TEMPORARY STORAGE OF THE LARGE CORE MEMORY REQUIREMENTS
   HAS BEEN IMPLEMENTED TO REDUCE THE COMPUTING COSTS
   BY BUFFERING DATA IN AND OUT OF CORE.
2) STANDARD BOEING INPUT FORMAT FOR THE WING SECTION
   HAS BEEN USED.
3) SUBPROGRAM BLIN HAS BEEN IMPLEMENTED TO ADD THE
   DISPLACEMENT THICKNESS TO THE ORIGINAL WING SECTIONS
4) WING SECTION LEADING EDGE SINGULAR POINT IS FOUND BY
   COMPUTING THE FOCUS OF A PARABOLA BY 2N+1 POINTS
   LEAST-SQUARE FIT CENTERED AT THE LEADING EDGE POINT.
   N IS SUPPLIED BY THE USER THROUGH INPUT CARD.
5) TRAILING EDGE CLOSURE ANGLE AND BISECTOR SLOPE ARE
   COMPUTED BASED ON BACKWARD DIFFERENCE.
6) OPTION FOR PRINTER-PLOTTING OF THE UNWRAPPED
   WING SECTIONS IS AVAILABLE
*****
THE FOLLOWING FILES ARE USED TO EXECUTE FLO27. SOME OF THESE
FILES ARE USED SUBSEQUENTLY IN OTHER MODULES OF THE VISCOUS/
INVISCID INTERACTIVE WING SYSTEM
FILE1 IS USED TO BUFFER DATA IN AND OUT OF CORE
FILE2 IS USED TO BUFFER DATA IN AND OUT OF CORE
FILE3 IS USED TO BUFFER DATA IN AND OUT OF CORE
*****
```



```

WRITE (6,52) K,NPCK,NPCK1,ZS(K)
WRITE (6,54) (DUMX(I),ZS(K),DUMY(I),I=1,NPCK)
CONTINUE 10
ENDFILE (1HQ,5X,3I5,F11.4/)
FORMAT (12F11.4)
CONTINUE
IF (KSYM.NE.0) YA = 0.
ISYM = ISYMO
IF (AL.NE.0) ISYM = 0
YAW = YA/RAD
SYAW = SIN(YAW)
CYAW = COS(YAW)
CA = CYAW*CSIN(ALPHA)
SA = CYAW*CSIN(ALPHA)
IF (FCCNT.LT.1.) GC TC 91
IF AC (4) = NX,NY,NZ,NM,K1,K2,NIT
MX = NX +1
MY = NY +2
MZ = NZ +3
DO 62 K=1,MZ
READ (4) ((G(I),J,I=1,MX),J=1,MY)
BUFFER (4) ((G(I),I),G(MX,MY,1))
WRITE (N3) ((G(I),J),I=1,MY)
IF (UNIT(N3).GT.0.) GO TO 1
BUFFER (N1) ((G(I),I),G(MX,MY,1))
WRITE (N1) ((G(I),J),I=1,MY)
IF (UNIT(N1).GT.0.) GO TO 1
CONTINUE (VORT(K),K=K1,K2)
READ (4)
REWIND N3
REWIND N1
REWIND 4
CALL CCCRD (NX,NY,NZ,KSYM,ZTIP,XLIM,ZLIM,
SY,AX,AZ,KSYM,KTE1,AC,BC,ZO)
CALL SINGL (NS,AZ,KSYM,KTE1,KTE2,FUS,CHCRD,ZS,XLE,YLE,
SWEEP,DIHED,XO,YO,ZO,YFO,ZPC,E1,E2,E3,IND)
CALL SUFF (ND,NET,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
YAW,XLIM,XP,YP,SN,D1,D2,D3,IND)
A0,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
SLOP1,TRAIL,
IF (INC.EC.C) GC TC 291
IF (FCCNT.GE.1.) GO TO 101
NM = 1
NIT = 0
CALL ESTIM
IF (IG.EC.0) GO TO 1

```

C C C C


```

RE WIND N1
RE WIND N1
IF (PTCK .GE. 1.0) WRITE (6,600)
FC CNT = 0
CO VG(NM)
P1 = P10(NM)
P2 = P20(NM)
P3 = P30(NM)
MIT = FIT(NM) +NIT
KIT (KIT.LT.2) KIT=2
JIT = NIT
LRES = 0
MRES = 0
NX +1
MY +2
MZ +3
KY +1
K1 = 1
K2 = NZ +1
IF (KSYM.EC.0) GO TC 103
K1 = NZ +3
K2 = NZ/2 +1
LZ = NZ +3
IF (KSYM.NE.0) LZ = 3
(PTCK .LE. 0.) GC TC 108
WRITE (6,104)
FORMAT (48H INDICATION OF LOCATION OF WING AND VORTEX SHEET,
27H IN CCGRDINATE PLANE Y = 0.,
27H ((IV(I,K),K=K1,K2),I=1,MX))
DO 106
WK ITE (6,650) (IV(I,K),K=K1,K2)
106 CONTINUE
IMAP = FTMAP(NM)
IF (IMAF .EQ. 0) GC TC 830
WRITE (6,112)
FORMAT (49H CHORDWISE CELL DISTRIBUTION IN SQUARE ROOT PLANE,
54H AND MAPPED SURFACE COORDINATES AT CENTER LINE AND TIP)
DO 820
ISEC = LZ/KTE2,IMAP
WRITE (6,812) ISEC,ZP0(ISEC)
FORMAT (15H I X ,20H SECTION PROFILE NO.,
1 I 2,3 P X Y (2,NX,A0,SO(1,ISEC))
820 CALL INLE
83C CONTINUE
LE. 0.) GC TC 130
WRITE (6,116)

```



```

116  FORMAT (15F0      TE LOCATION ,15H      PCWER LAW )
      WRITE (6,610) XLIM,AX
      WRITE (6,60C)
      WRITE (6,118)
118  FORMAT (46HONORMAL CELL DISTRIBUTION IN SQUARE ROOT PLANE/
      15F0
      DO 120      =1,KY
120  WRITE (6,61C) BC(J)
      WRITE (6,122)
122  FORMAT (15F0      SCALE FACTOR,15H      PCWER LAW )
      WRITE (6,61C) SY,AY
      WRITE (6,600)
      WRITE (6,124)
124  FORMAT (45HOSPANWISE CELL DISTRIBUTION AND SINGULAR LINE/
      15H0      X SING ,15H      Y SING )
      DO 126      K=K1,K2
126  WRITE (6,61C) ZO(K),XO(K),YO(K)
      WRITE (6,128)
128  FORMAT (15H0      TIP LCCATION,15H      PCWER LAW )
      WRITE (6,61C) ZLIM,AZ
130  CONTINUE
      WRITE (6,60C)
      WRITE (6,132)
132  FORMAT (15H0ITERATIVE SCLUTION)
      WRITE (6,134)
134  FORMAT (15H0      MACH NO ,15H      YAW ,15H      ANG OF ATTACK)
      WRITE (6,610) FMACH,YA,AL
      WRITE (6,136) NX
      WRITE (6,130) NX,NY,NZ
      WRITE (6,640)
      WRITE (6,138)
138  FORMAT (15H0      RELAX FCT 1 ,15H      RELAX FCT 2 ,15H      RELAX FCT 3 )
      WRITE (6,610) P10(NM),P20(NM),P30(NM)
      WRITE (6,140)
140  FORMAT (10H0ITERATION,
      15H      MAX CORREC N ,4H      I ,4H      J ,4H      K ,15H      AVG CORREC N ;
      15H      MAX RESIDUAL ,4H      I ,4H      J ,4H      K ,15H      AVG RESIDAL ;
      12H      CIRCULATION,15H      SONIC PIS)
      WRITE (6,140)
141  NIT
      JIT
      CALL MIXFLC
      IF (10.EC.0) GO TO 151
      JO
      REWIND N1
      REWIND N2
      N1
      N1
      N2
      N2
      N3
      N3

```



```

N3
WRITE (6,66C) NIT, DG, IG, JG, KG, AG, FRES, JFES, JRES, KRES, ARES,
1
LRES = LRES
IF (LRES.EQ.MRES) LRES = 1
IF (LRES.NE.1) GO TO 143
NRRES = NRRES + 1
COUNT(NRES) = NRES - 1
RES(NRES) = FRES
IF (JIT.GE.KIT) GO TO 251
IF (NM.LE.1 .OR. NM.LT.MMESH) GO TO 148
IF (ABS(DG) .LE. COV) GO TO 251
143 CONTINUE
IF (NINI.LT.MIT .AND. ABS(DG).GT.COV .AND. ABS(DG).LT.10.) GO TO 141
GO TO 161
IF (JOREC.1) GO TO 1
REWIND A1
REWIND A2
JO
N
N3
N2
N1
GO TO 141
161 RATE = 0.
IF (NRES.GT.1) RATE = (ABS(RES(NRES)/RES(1)))
* (1./((COUNT(NRES) - COUNT(1))))
162 WRITE (6,162) MAX RESIDUAL 1,15H MAX RESIDUAL 2,15H
FORMAT (15H0 MAX REDUCTN/CYCLE, 15H CONV TOLERANCE)
1 WRITE (6,670) RES(1), RES(NRES), COUNT(NRES), RATE
1,CCV
WRITE (6,600)
DO 164 M=1,3
BUFFER IN (N1, 1) (G(1,1,M), G(MX,MY,M))
READ (N1,ERR=151) ((G(I,J,M), I=1,MX), J=1,MY)
IF (UNIT(N1).GT.0.) GO TO 151
CONTINUE
LX = NX/2 + 1
K = 2
KKK = 0
WRITE HEADER CN TAPE 8
IF (NM.LT.MMESH) GO TO 17C
REWIND 8
REWIND 9
NRC = KIE2 - KIE1 + 1
WRITE (8) (TITLE(I), I=1,8), FMACH, ALPHA, NRC
17C CONTINUE

```

WORK


```

171 K = K + 1
    IF (K.EC.MZ) GO TO 191
    DO 172 J=1,MX
    DO 172 I=1,MY
    G(I,J,1) = G(I,J,3)
    G(I,J,2) = G(I,J,1)
    BUFFER IN (N1,ERR=151) ((G(I,J,3),I=1,MX),J=1,MY)
    READ (N1,ERR=151) (GO TO 151)
    IF (UNIT(N1).GT.0.) GO TO 151
    IF (K.LT.KTEL.OR.K.GT.KTE2) GO TO 171
    CALL VELD (KTEL,SV,SM,CP,XP,YP,XMAX(K),XMIN(K),YMAX(K),YMIN(K))
    I1 = ITEL(K)
    I2 = ITE2(K)
    CHCRD(K) = XP(I1) -XP(LX)
    CALL FCRCF (I1,I2,XP,YP,CP,AL,CHORD(K),XO(K),YPO(K),
    SCL(K),SCD(K),SCM(K))
1 KKK = KKK + 1
    IF (KPLCT.GT.1.AND.K.GT.KTEL) GC TC 185
    IF (KPLCT.EQ.0.AND.KKK.GT.1) GO TO 185
    WRITE (6,600)
    WRITE (6,182)
182 FORMAT(24HOSECTION CHARACTERISTICS/
    MACH NO ,15H YAW
    ,15H ANG OF ATTACK)
184 WRITE (6,610) FMACH,YA,AL CL
    WRITE (6,184) HOSPAN STATION ,15H CD
185 FORMAT(15H CM
    ,15H ANG OF ATTACK)
    WRITE (6,610) ZPO(K),SCL(K),SCD(K),SCM(K)
    Z = ZPC(K)
    IF (MIT.LE.0) GC TO 850
    IF (KPLCT.LE.2) CALL CPLOT (2,NX,FMACH,XP,YF,CP,SM,I1,I2,KPLOT)
    C 850 CONTINUE
        WRITE CNE FILE ON TAPE 8
        IF (NM.LT.MMESH) GO TO 186
        WRITE (8) NCI
        WRITE (8) (XT3(I),YT3(I),VT3(I),WT3(I),VT3(J),I=1,NOI)
        NRC=I2-I1+1
        C 850 CONTINUE
            WRITE CP VS X/C SECTION DATA FOR FINAL MESH ON TAPE 9
            WRITE (9,900) ZPO(K)
            WRITE (9,910) NRD
            WRITE (9,920)
            WRITE (9,950) (XCD(J),CP(J),J=1,I2)
            FORMAT (/,14HSPAN STATION =,F12.5)
            FORMAT (1X,20HNC. CF DATA POINTS =,I5)
            FORMAT (1X,6H X/C,8X,2HCP,7X,3HX/C,8X,2HCF,7X,3HX/C,8X,2HCP,
            17X,3HX/C,8X,2HCF,3X)
            WRITE (8F10.6)
            C 850 CONTINUE

```



```

C WHEN KPLOT = 2 CALL SUBROUTINE VERTEC WHICH PLOTS CP VS X/C
C FOR EACH SECTION OF THE FINAL MESH
C
1 IF (KPLCT.EC.2.AND.NM.EQ.MMESH) CALL VERTEC(I1,I2,XOCD,CP,NRD,
ZPO,FMACH,YA,AL,SCL,SCD,SCM,K)
1 GO TO 171
CONTINUE
191 IF (NM.LT.MMESH) GO TC 200
ENCFILE 8
REWIND 8
ENDFILE 5
REWIND 5
CONTINUE
200 CALL TCTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,XC,YPO,ZPO,
CL,CDI,CMP,CMR,CMY,
CYAW*CDI
=CDO +CDI
=0
VLCI
IF (ABS(CDI).GT.1.E-6) VLD1 = CL/CDI
VLC
IF (ABS(CD).GT.1.E-6) VLD = CL/CD
WRITE (6,60C)
WRITE (6,192)
FORMAT (21H) MACH NO ,15H YAW
192 1 15H0 FMACH,YA,AL
WRITE (6,610) CL ,15H CD FORM
WRITE (6,154) CD ,15H L/C FORM
FORMAT (15H) CL,CDI,CDO,CD,VLD1,VLD
194 1 15H0 CM YAW ,15H CM RCLL
WRITE (6,610) CMY,CMR,CMP
REWIND 1
IF (KPLCT.LT.1) GO TO 201
CALL RPLCT (IPLCT,NRES,COUNT,TITLE,FMACH,YA,AL,NX,NY,NZ)
CALL DRAW (IPLCT,XMAX,XMIN,YMIN,ZPO,FUS,TITLE,NZ,KTE1,KTE2)
CALL TPREED (IPLCT,SV,SM,CP,XP,YP,ZPO,TITLE,YA,AL,
VLC,CL,CD,CHORDO,XSCAL,PSCAL)
1 IF (IO.EQ.0) GO TO 151
IF (ISICP.EQ.1) GO TO 301
IF (NM.LT.MMESH) GC TC 203
GO TO 1
CONTINUE
NX = NX +NX
NY = NY +NY
NZ = NZ +NZ

```



```

CALL CCCRD (NX, NY, NZ, KSYM, ZTIP, XLIM, ZLIM,
1 SY, AX, AZ, PX, PZ, AO, BC, ZO)
CALL SINGL (NS, NZ, KSYM, KTE1, KTE2, FUS, CHRDO, ZS, XLE, YLE,
1 SWEEP, DIHED, XO, YO, ZC, YPC, ZPC, E1, E2, E3, IND)
CALL SUFF (ND, NE, NS, NX, NZ, ISYM, KSYM, KTE1, KTE2,
1 YAW, XTEQ, XLIM, FIX, NP, XS, SLOP, TRAIL,
2 AO, XO, ZO, SO, SCAL, ZV, IV, ITE1, ITE2,
3 XP, YP, SN, CI, D2, D3, IND)
IF (INC.EQ.0) GC IC 291
CALL REFIN
IF (IO.EQ.0) GO TO 221
REWIND N1
REWIND N2
NSMOO = FSMCC(NM)
IF (NSMCC.LT.1) GO TO 211
DO 202 N=1, NSMCC
CALL SMCC
IF (IO.EQ.0) GO TO 221
REWIND N1
REWIND N2
202 N1 = N1
211 N1 = N2
N2 = N3
N3 = NM +1
NM = 0
NIT TO 101
GO TO 101
221 NX = NX/2
NY = NY/2
NZ = NZ/2
CALL CCCRD (NX, NY, NZ, KSYM, ZTIP, XLIM, ZLIM,
1 SY, AX, AZ, PX, PZ, AO, BC, ZO)
CALL SINGL (NS, NZ, KSYM, KTE1, KTE2, FUS, CHRDO, ZS, XLE, YLE,
1 SWEEP, DIHED, XO, YO, ZC, YPC, ZPC, E1, E2, E3, IND)
CALL SLRF (ND, NE, NS, NX, NZ, ISYM, KSYM, KTE1, KTE2,
1 YAW, XTEQ, XLIM, FIX, NP, XS, SLOP, TRAIL,
2 AO, XO, ZO, SO, SCAL, ZV, IV, ITE1, ITE2,
3 XP, YP, SN, CI, D2, D3, IND)
IF (INC.EQ.0) GC IC 291
GO TO 151
251 K1 = KTE1 -1
K2 = KTE2 +1
WRITE (14) NX, NY, NZ, NM, K1, K2, NIT
DO 262 K=1, NZ
BUFFER IN ERR=281 ((G(I, J, I), I=1, MX), J=1, MY)
READ (N1) (N1) GT.0. GO TO 281
IF (UN1(N1)) (G(I, J, I), I=1, MX), J=1, MY)
262 WRITE (14) ((G(I, J, I), I=1, MX), J=1, MY)

```



```

REWIND A1 (VORT(K),K=K1,K2)
WRITE (14)
ENDFILE 14
REWIND SWITCH(1,ISTOP)
CALL SLIET(1,ISTOP)
IF (ISTCP.EC.1) GO TO 161
JI 7
IF (NI7.LT.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GC TO 141
GO TO 161
REWIND 4
281 GO TO 151
291 WRITE (6,600)
292 WRITE (6,292)
292 FORMAT(24HOBAD DATA,SPLINE FAILURE)
301 GO TO 1
CONTINUE
REWIND 11
IF (KPLCT.GT.0) CALL PLOT(0.,0.,955)
STCP
50C FORMAT(1X)
51C FORMAT(8F10.6)
53C FORMAT(2CA4)
60C FORMAT(1H1) 5,7G15.5)
61C FORMAT(F12.20A4)
63C FORMAT(1H0,7I15)
64C FORMAT(1X,3I13)
65C FORMAT(1I10,E15.5,3I4,E15.5,F10.5,I10,F10.3)
660 FORMAT(2E15.4,2F15.4,E15.4)
67C END

```



```

IF (I.LT.NL) SI = -1.
GO TO 850
820 CONTINUE
S = 0.
DL = DELR(I)
DX = 0.
DY = DL*SI
GO TO 880
850 CONTINUE + DYXN**2
S = SQR1(S)
S = 1./S
F = 1.
IF (DYXN *SI.LT.0.) F = -1.
DL = DELR(I)
DX = S*F
DY = ABS(DYXN)*S*SI
DY = DY * DL
XT(I) = X2 + DX*WEIG
YT(I) = Y2 + DY*WEIG
880 CONTINUE
IF (PTCK .LE. 1.) GO TO 890
WRITE (C,1000) I,F,S,DL,DX,DY,CYXN,XT(I),YT(I),DYX,WEIG
890 CONTINUE
IF (I.EC.N) GO TO 900
X1 = X2
Y1 = Y2
X2 = X3
Y2 = Y3
I = I + 1
GO TO 200
900 CONTINUE
RETURN
1000 FORMAT (1H ,I5,F7.2,9G13.5)
END

```



```

C**SUBROUTINE PPXY*****
SUBROUTINE PPXY (I1,I2,X,Y)
C
C SUBPRGAM FCR LINE PRINTER PLOTTING OF THE UNWRAPPED
C WING SECTIONS
COMMON /PCKR/ PTCK
COMMON /SHARE/ LINE(100)
DIMENS ICN X(1),Y(1)
DATA IB /1H /, IP /1H+/, KMAX /100/, ACC /1.5/,
1 IZ /1F/, ICONST /0/
DO 10 I=1,100
LINE(I) = IB
10 CONTINUE
YMAX = -1.0E35
YMIN = -YMAX
WICTH = KMAX - 5
DO 20 I = 11,I2
YMAX = AMAX1(YMAX,Y(I))
YMIN = AMIN1(YMIN,Y(I))
20 CONTINUE
VAL = ABS(YMAX) + ABS(YMIN)
S = WICTH/VAL
KK = ICONST.LE.YMAX .AND. ICONST.GE.YMIN) KK = S*(YMAX-ICONST)+ADD
IF (KK.NE.0) LINE(KK)=IZ
DO 30 I=11,I2
K = (YMAX-Y(I)) + ADD
IF (K.LT.1) K = 1
IF (K.GT.KMAX) K = KMAX
LINE(K) = IP
WRITE(K) (E,100) I,X(I),Y(I),LINE
LINE(K) = IB
IF (K.EC.KK) LINE(KK) = IZ
30 CONTINUE
RETURN
100 FORMAT (1X,I3,2F10.4,4X,100A1)
ENC

```



```

C**SUBROUTINE LSQR***(NL,NB,XP,YP,XSING,YSING)
SUBROUTINE LSQR (NL,NB,XP,YP,XSING,YSING)
SUBPROGRAM FOR WING SECTION LEADING EDGE SINGULAR POINT
CALCULATION BY MEANS OF COMPUTING THE FOCUS OF A
PARABOLA BY NB*(Z+1) POINTS LEAST-SQUARE FIT CENTERED AT
THE LEADING EDGE
NB: SUPPLY BY THE CALLING PROGRAM GEOM
COMMON /FCKR/ FTCK
DIMENSION XP(1),YP(1)
N1 = NL - NB
N2 = NL + NB
N = N2 - N1 + 1
A1 = N
B1 = 0.
C1 = 0.
A2 = 0.
B2 = 0.
C2 = 0.
A3 = 0.
B3 = 0.
C3 = 0.
D1 = 0.
D2 = 0.
D3 = 0.
SCALE1 = 100.
SCALE2 = 500.
DO 300 I = N1,N2
YY = (YP(I) - YP(NL))*SCALE
B1 = B1 + YY
C1 = C1 + YP2
YP3 = C2 + YP3
YP4 = C3 + YP4
CX = XP(I) * SCALE
CY = D1 + YX * X
DY = D2 + YX * XX
Y2X = D3 + YF2 + Y2X
D3 = D3 - B1
A2 = A2 - C1
A3 = A3 - C2
B3

```

30C


```

B2*C3 - B2*C2
FA2*FA3 - A3*FA2 + C1*FA3
DEI = 1
FA2 = 1
FA3 = 1
FB1 = 1
FB2 = 1
FB3 = 1
FC1 = 1
FC2 = 1
FC3 = 1
A = 1
B = 1
C = 1
X = 1
Y = 1
Z = 1
...
400 1
500
520
...

```



```

DXAM = CXA
DXAM = CXA
DX2M = CXAM**2
60C CONTINUE LE= 0.) GC TC 65C
WRITE (6,70C) I,X,Y,DX,DX2,R2,CXAM,DX2M,XP(I),YP(I)
65C CONTINUE LE= 0.) GC TC 75C
IF (PTICK .LE. 0.) GC TC 75C
RA = R2/A1
WRITE (6,70C) N,RA,DXAM
70C FORMAT (113,9G13.5)
CONTINUE
RETURN LSC
IF (DXAM .LE. 1.E-4) RETURN
WRITE (6,80C) DXAM
80C FORMAT (1H0,5X,'WARNING ??? DEVIATION OF THE LEADING EDGE PCINIS',
1 FROM PARABOLA IS GREATER THAN 0.C001/6X,'DXAM =',G13.4//)
RETURN
END

```



```

C** SUBROUTINE GEOM** (ND, NS, NP, XS, YS, ZS, XLE, YLE, SLOPI, TRAIL, XP, YP,
SUBROUTINE GEOM (ND, NS, NP, XS, YS, ZS, XLE, YLE, SLOPI, TRAIL, XP, YP,
1 FIX, PX, PZ, I SYMO, KSYM)
2
C** GEOMETRIC DEFINITION OF WING
C** STANDARD BOEING INPUT FORMAT FOR WING SECTION DATA IS USED
C** OPTION FOR WING SECTION TRAILING EDGE CLOSURE ANGLE
C** AND BISECTOR SLOP BE AUTOMATIC COMPUTED IS AVAILABLE
C** LEADING EDGE SINGULAR POINT CAN BE AUTOMATIC CCNPUTED
C** BY INVCKING THE OPTION TO CALL LSQR
C** COMMON /PCPKR/ PTCK
C** COMMON /CCPF/ NL
C** DIMENSION XS(ND, 1), YS(ND, 1), ZS(1), XLE(1), YLE(1),
1 SLOPT(1), TRAIL(1), XP(ND), YP(ND), NP(1)
C** INITIALIZE INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES **
C**
FNB = 2.0
PX = 0.0
PZ = 0.0
FRLX = 0.0
SLTL = 0.0
XSING = 0.0
YSYM = 0.0
C**
RAD = 57.255779513082
READ (5, 500)
READ (5, 510) ZSYM, FNS, SWEEP, DIHED, FUS
IF (FNS.LT.3.) RETURN
KSYM = ZSYM
IF (FUS.GE.0.) KSYM = 1
NS = FNS
WRITE (6, 2) FUSELAGE RAD )
2 FORMAT (15F0 FUSELAGE RAD )
WRITE (6, 4) SWEEP, DIHED
4 FORMAT (15H SWEEP, DIHED
WRITE (6, 10) SWEEP/RAD
SWEEP/RAD
DIHED/RAD
DIHED/RAD

```



```

ISYMO      = 1
XTEC      = 0.
CHORDO    = 0.
K         = 1
11 READ   (5,500) ZS(K),XL,YL,CHORD,THICK,AL,FSEC
READ      (5,510) ZS1 = ZS(1)
IF (K.EC.1) ZS1 = AL/RAD
ALPHA     = AL/RAD
IF (K.GT.1.AND.FSEC.EQ.0.) GO TO 31
READ      (5,500)
READ      (5,510) FN
N         = FN
READ      (5,500)
N1 = N + 1
READ      (5,520) (XF(N1-1),YP(N1-1),I=1,N)
FORMAT    (6F10.0)
DO 26 I=1,N
IF (XP(I+1).LT.XP(I)) GC TC 26
NL = I
GO TO 800
CONTINUE
IF (FNE.LE.0.) GC TO 21
DYL = YF(1) - YF(2)
DXL = XF(1) - XF(2)
DYU = YF(N) - YF(N-1)
DXU = XF(N) - XF(N-1)
TSL = CYL/DXU
TRL = ATAN2(DYL,DXL) - ATAN2(DYU,DXU)
SLT = (1SL+TSU)*.5
NB = FNE
CALL LSCR (NL,NE,XP,YP,XSING,YSING)
21 WRITE  (6,600) ZS(K)
WRITE    (6,620) NL,XP(NL),YP(NL) = ,I3,,XP(NL) = ,F10.5 // (XP,YP) //
22 FORMAT (16F10.0)
WRITE   (6,610) TRL,SLT,XSING,YSING
WRITE   (6,620) NL,XP(NL),YP(NL) = ,I3,,XP(NL) = ,F10.5 // (XP,YP) //
22 FORMAT (16F10.0,4X) )
WRITE   (6,610) TRL,SLT,XSING,YSING
WRITE   (6,620) NL,XP(NL),YP(NL) = ,I3,,XP(NL) = ,F10.5 // (XP,YP) //
31 SCALE (2X,5
XLE(K) = XL + (XSING -XP(NL)) *THICK*SCALE
YLE(K) = YL + (YSING -YP(NL)) *THICK*SCALE
XX     = XP(NL) + (XSING -XP(NL)) *THICK
YY     = YP(NL) + (YSING -YP(NL)) *THICK

```



```

CA      = COS(ALPHA)
SA      = SIN(ALPHA)
DO 22 I=1,N
XS(I,K) = SCALE*((XP(I) -XX)*CA +THICK*(YP(I) -YY)*SA)
YS(I,K) = SCALE*(THICK*(YP(I) -YY)*CA -(XP(I) -XX)*SA)
32 SLOP(I,K) = THICK*SLT -TAN(ALPHA)
TRAIL(K) = N
NP(K) = N
CHORDO = AMAX1(CHORDO,CHORD)
IF (YS(YA*LE*0.0,CR.ALPHA*NE*0.0) ISYMC = C
WRITE (6,42) ZS(K)
42 FORMAT (27F10.5)
15H SECTION DEFINITION AT Z = ,F10.5/ ,15H
15H THICKNESS RATIO,15H
15H XLE ,15H
15H YL,CHCRD,THICK,AL
WRITE (6,610) XL,YL,CHCRD,THICK,AL
YMIN = YP(NL)
YMAX = YMIN
DO 44 I = 1,N
IF (YP(I) .GE. YMIN) GC TO 43
JMIN = I
YMIN = YP(I)
43 IF (YP(I) .LE. YMAX) GC TO 44
YMAX = YP(I)
44 CONTINUE
YDIF = YMAX - YMIN
NN = N - 1
SUM = 0.
DO 46 I = NL,NN
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
46 CONTINUE
NM = 1
DO 48 I = 1,NM
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
48 CONTINUE
30C 15H
WRITE (6,300) JMAX YMIN ,15H JMIN ,15H YDIF ,15H
FORMAT (15H JMAX ,15H YMIN ,15H JMIN ,15H YDIF ,15H
320 CALL LSC
IF (FUS*LE*0.) GO TO 61
R = AMAX1(0.,ZSI + SQRTR)
Z = ZS(K) = FUS**2/(YLE(K)**2 +Z**2)
RZS(K) = Z*(1.-R)
YLE(K) = YLE(K)*(1.+R)
S = R*XS(NL,K)

```

CHORD

YMAX

AREA


```

XLE(K) = XLE(K) -S
DO 52 I=1,N
XS(I,K) = XS(I,K) +S
YS(I,K) = YS(I,K) * (1. +R)
52 K = K +I
IF (K.LE.NS) GO TO 11
Z0 = ZS(1) +ZS(NS)
IF (KSYM.NE.0) Z0 = ZS(1)
DO 62 K=1,NS
XTEO = AMAX1(XTEO,XS(1,K))
ZS(K) = Z0
62 ZTIP = ZS(NS)
RETURN
FORMAT(1X)
500 FORMAT(8F10.6)
510 FORMAT(1H1)
60C FORMAT(F12.4,7F15.4)
61C ENC

```



```

C**SUBROUTINE COORD**
SUBROUTINE COORD (NX,NY,NZ,KS,SYM,ZIIP,XLIM,ZLIM,
SY,AX,AZ,PX,PZ,AO,BO,ZO)
SETS UP STRETCHED PARABOLIC AND SPANWISE COORDINATES
DIMENSION AO(1),BO(1),ZO(1)
PI = 3.1415926535898
BOUND = .95
AX = .5
AY = .5
AZ = .5
XLIM = .625*BCUND
ZLIM = .625*BCUND
SY = 5
SCALZ = ZIIP/(1.000001*ZLIM)
LX = NX/2 + 1
NX = NX * BCUNC/NX
DX = PI/XLIM
Q = PX/C
R = 1./(1. + R*SIN(Q) - XLIM)
DO 12 I=1,MX
C = (I - LX)*DX
D = D + R*SIN(C*D)
IF (ABS(D).LE.XLIM) GO TO 12
B = 1.
A = 1.
C = A**AX
D = B**XLIM + (D - B**XLIM)/C
12 AO(I) = D
DY = NY + 1
DO 22 J=1,KY
D = (KY - J)*DY
A = 1.
C = A**AY
D = SY*D/C
22 BO(J) = D
LZ = 1
K1 = 1
K2 = 1
DZ = 1
R = (KSYM.EC.0) GO TC 31
IF LZ = 3
K1 = 2
K2 = 2
NZ = NZ + 3
BOUND = NZ

```



```

31  Q R E DO 32 K=K1,K2      +Q      +R*SIN(Q)  -ZLIM)
    = -PZ/Q
    = 1./((1.
    = (K  -LZ)*DZ
    = D  +R*SIN(C*D)
    B IF (ABS(C).LE.ZLIM) GC TO 32
    = 1.
    A IF (D.LT.0.) B = -1.
    = 1.  -(C  -B*ZLIM)*E)**2
    = A**AZ
    = B*ZLIM  +(D  -B*ZLIM)/C
    = SCALZ*C
32  ZO(K)
    RETURN
    END

```



```

C**SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRDO,ZS,XLE,YLE,
SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRDO,ZS,XLE,YLE,
1 GENERATES SINGULAR LINE FOR SQUARE ROOT TRANSFORMATION
DIMENSION ZS(1),X0(1),Y0(1),ZC(1),XLE(1),E2,E3,IND)
1 EL(1),E2(1),E3(1)
K1 = NZ +1
K2 = NZ +2
K3 = NZ +3
KTE1 = K1
KTE2 = K2
11 DO 12 K=K1,K2
IF (ZC(K).LT.ZS(1)) KTE1 = K +1
IF (ZC(K).LE.ZS(NS)) KTE2 = K
12 CONTINUE
CALL SFLIF (1,NS,ZS,XLE,E1,E2,E3,2,0,2,0,0,0,IND)
CALL INTPL (KTE1,KTE2,ZO,XO,1,NS,ZS,XLE,E1,E2,E3,0)
S = CHORDO*EI(1)
S1 = CHORDO*EI(1)
S2 = CHORDO*EI(NS)
CALL SFLIF (1,NS,ZS,YLE,E1,E2,E3,2,0,2,0,0,0,IND)
CALL INTPL (KTE1,KTE2,ZO,YO,1,NS,ZS,YLE,E1,E2,E3,0)
T1 = CHORDO*EI(1)
T2 = CHORDO*EI(NS)
XO(KTE1-1) = XO(KTE1) -XO(KTE1+1)
YO(KTE1-1) = YO(KTE1) -YO(KTE1+1)
IF (KSYM.NE.0) GO TO 31
N = KTE1 -1
DU 22 K=K1,N
ZZ = (ZO(K) -ZO(KTE1))/CHORDO
A = EXP(ZZ)
XO(K) = XO(KTE1) +S*ZZ -(S1 -S)*A
YO(K) = YO(KTE1) +T*ZZ -(T1 -T)*A
31 N DO 32 K=N,K2
ZZ = (ZO(K) -ZO(KTE2))/CHORDO
A = EXP(-ZZ)
XO(K) = XO(KTE2) +S*ZZ +(S2 -S)*A
YO(K) = YO(KTE2) +T*ZZ +(T2 -T)*A
32 DO 42 K=K1,K2
YPO(K) = YO(K)
ZPC(K) = ZO(K)
IF (FUS.LE.0) GO TO 42
A = .25*(ZO(K)**2 -YO(K)**2) +FUS**2
B = .5*ZO(K)*YO(K)
S = SQRT(A**2 +B**2)

```



```
T = 0
IF (S.GT.0.) T = .5*ATAN2(B,A)
S = Sqrt(S)
YPO(K) = .5*Y0(K) + S*SIN(T)
ZPO(K) = .5*Z0(K) + S*COS(T)
CONTINUE
RETURN
ENC
```

42


```

DO 42 I=1,N
R   = SQRT(XS(I, KK)**2 +YS(I, KK)**2)
IF (R.EC.C.) GO TO 43
ANGL = ATAN2((U*YS(I, KK) -V*XS(I, KK)),
             (U*XS(I, KK) +V*YS(I, KK)))
1  U   = XS(I, KK)
V   = YS(I, KK)
R   = SQRT(R +R)
XP(I) = R*.5*ANGL
YP(I) = R*.5*ANGL
GO TO 42
42 ANGL = PI
U   = -1.
V   = 0.
R   = 0.
CONTINUE
SS   = AO(I2)/AMIN1(ABS(XP(I)),ABS(XP(N)))
DO 44 I=1,N
XP(I) = S*XF(I)
YP(I) = S*YF(I)
ANGL1 = ATAN(SLOPT(KK))
ANGL2 = ATAN(YS(I, KK)/XS(I, KK))
ANGL1 = ATAN(YS(N, KK)/XS(N, KK))
ANGL2 = ATAN(.5*(ANGL1 -IRAIL(KK)))
T1    = ANGL - .5*(ANGL2 +TRAIL(KK))
T2    = TAN(ANGL1)
TAN(ANGL2)
CALL SFLIF (I, N, XP, YP, D1, D2, D3, I, T1, I, T2, O, O, IND)
IF (INC.EC.O) WRITE(6, 500) KK, K1, K2, N, FR, R1, R2, ZS(KK)
500 FORMAT (I2, HOBA, D, MA, PING, 4, I10, 4, G13.4/)
CALL INTPL (I1, I2, AO, SA, I, A, XP, YP, C1, D2, D3, C)
X1    = .25*XS(I, KK)
A     = SLOPT(KK)*XS(I, KK) -X1)
B     = PI/(XS(I, KK) -X1)
ANGL = 1.
U     = 0.
V     = 0.
M     = I1 -1
DO 52 I=2,M
XX    = SS*AO(I)**2
D     = B*(XX -X1) +A*ALOG(D)/D
Y     = YS(I, KK)**2 +YY**2
R     = SQRT(XX**2 +ATAN2((U*YY -V*XX), (U*XX +V*YY)))
ANGL = ANGL
U     = XX
V     = YY

```



```

52 SN(I) = S*SCRT(R +R)
A = R*SIN(.5*ANGL)
B = SLGFT(KK)*(XS(N,KK) -X1)
U = 1./(XS(N,KK) -X1)
V = 0.
M = 0.
DO 54 I=M,NX +1
XX = SS*AO(I)**2
D = B*(XX -X1)
YY = YS(N,KK) + A*ALOG(D)/D
R = SQRT(XX**2 +YY**2)
U ANGL = ANGL +ATAN2((U*YY -V*XX),(U*XX +V*YY))
U V = YY
R = S*SCRT(R +R)
54 SN(I) = R*SIN(.5*ANGL)
62 DO 62 I=2,NX
SO(I,K) = SO(I,K) +RR*SN(I)
IF (KK.EC.K2) GC TC 71
KK = K2
RR = R2
GO TO 41 = SS0
71 IF (FIX.EQ.0.) = (R1*XS(1,K1) +R2*XS(1,K2))/(A0(I1)**2 -S0(I1,K)**2)
1SS = SS +SS
SCAL(K) = SS
ITE1(K) = I1
ITE2(K) = I2
ZV(K) = ZO(K) -TYAW*(X0(K) +SS*AC(I1)*A0(I1))
DO 72 I=I1,I2
IV(I,K) = I1 -1
72 M DO 74 I=1,M
ZZ = ZO(K) -TYAW*(X0(K) +SS*AO(I)*A0(I))
IF (ZZ.GE.ZV(KTEL)) IV(I,K) = IVO
74 M CONTINUE = I2 +1
DO 76 I=M,MX
ZZ = ZO(K) -TYAW*(X0(K) +SS*AO(I)*A0(I))
IF (ZZ.GE.ZV(KTEL)) IV(I,K) = IVO
76 M CONTINUE = K2 -1
K = K +1
IF (K.LE.KTE2) GC TC 21
K1 = 2
K2 = NZ

```



```

IF (KSYM.EQ.0) GC TC 81
K1 = NZ
K2 = NZ +2
81 SCAL(K) = SCAL(KTE2)
DO 82 I=1,MX
ZZ = ZO(K) -TYAW*(X0(K) +SS*A0(I)*A0(I))
IF (ZZ.LE.ZS(NS).AND.ZZ.GE.ZV(KTE1)) IV(I,K) = IVO
82 CONTINUE
K = K +1
IF (K.LE.K2) GO TO 81
SCAL(K) = SCAL(KTE2)
N = KTE2
IF (YAW.LE.0.) GO TO 93
DO 92 I=10,LX
N = N +1
92 ZV(N) = ZO(KTE2) -TYAW*(X0(KTE2) +SS*A0(I)*A0(I))
93 ZV(N+1) = ZTE1(KTE1)
ZV(N+1) = ZO(KTE2+1)
DO 102 K=K1,K2
DO 104 I=2,NX
IF (IV(I,K).GT.0) GC TC 104
IF (IV(I+1,K+1).GT.C.OR.IV(I-1,K+1).GT.C) IV(I,K) = IV1
IF (IV(I+1,K-1).GT.0.OR.IV(I-1,K-1).GT.C) IV(I,K) = IV1
104 CONTINUE
IF (SO(LX,K).LT.1.E-05) IV(LX,K) = 0
102 IF (KSYM.NE.0) RETURN
N = KTE1 -1
DO 112 K=1,N
SCAL(K) = SCAL(KTE1)
112 RETURN
ENC

```



```

C**SUBROUTINE ESTIM**
C**SUPERROUTINE ESTIM**
C**INITIAL ESTIMATE OF REDUCED POTENTIAL**
C**COMMON**
C**1 IV(161,18,3), SO(161,35), VORI(115), ZV(115),**
C**2 AO(161,18), IITE1(35), IITE2(35),**
C**3 NX,NY,NZ, KTE1, XO(35), YC(35), ZC(35), SCAL(35),**
C**4 YA,W,CY,Ah, SYAW, ALPHA, CA, SA, FMACH, N1, N2, N3, IC**
C**= NX +1**
C**= NY +2**
C**= NZ +3**
C**DO 12 I=1,161**
C**DO 12 J=1,18**
C**DO 12 K=1,3 O. MZ**
C**G(I,J,K) = 0. ((G(I,J,I), I=1, MX), J=1, MY)**
C**WRITE (N1) ((G(I,J,I), I=1, MX), J=1, MY)**
C**CONTINUE**
C**K1 = KTE1 -1**
C**K2 = KTE2 +IITE2(KTE2) -NX/2**
C**DO 32 K=K1, K2**
C**VORT(K) = 0. = 1**
C**IO RETURN**
C**END**

```



```

C**SUBROUTINE MIXFLO*****
SUBROUTINE MIXFLO*****
SOLUTION LINE EQUATION SCHEME FOR MIXED SUBSONIC AND SUPERSONIC FLOW
USING FINITE VOLUME SCHEME
COMMON
1 IV(161,18,3), SO(161,35), VORT(115), ZV(115),
2 AO(161,35), ITE1(35), ITE2(35), Z0(35), SCAL(35),
3 NX,NY,NZ,KTEL,KTE2,ISYM,KSYM,FUS,
4 YAW,CYAW,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,I0
COMMON/SPA/
1 GL(161,18), QQL(161,18), FL(161,18),
2 UL(161,18), VL(161,18), WL(161,18),
3 AL(161,18), BL(161,18), CL(161,18),
COMMON/FLC/
1 RI,IP2,IP3,FRES, IRES, JRES, KRES, ARES, DG, IG, JG, KG, AG, NSUP
COMMON/SWP/
1 K,NV,LX, MX, KY, MY, JI, KI, FMACH2, AAO, Q1, Q2, RV, TYAW, TOT
LX = NX/2 +1
KY = NY +1
MY = NY +2
JI = 2
IF (FMACH.GE.1.) JI = 3
TYAW = SYAW/CYAW
FMACH2 = FMACH*2
AAO = 1./FMACH*2 +.2
Q1 = 2./F1
Q2 = 1./FP2 -1.
TOT = 0.
FRES = 0.
ARES = 0.
DG = 0.
AG = 0.
NSUP = 0
K1 = 3
K2 = NZ +2
IF (KSYM.EQ.1) GO TO 1
IF (FMACH.GE.1.) K1 = 3
K2 = NZ
1 DO 2 M=2,3
2 READ (NI,ERR=101) ((G(I,J,M), I=1,MX), J=1,MY)
CONTINUE
K
NV = 1
RV = KTEL -1
DO 12 I=1,MY
DO 12 J=1,MX
G(I,J,1) = G(I,J,2)
GL(I,J) = G(I,J,2)

```



```

12  QQL(I,J) = 0.
    FL(I,J) = 0.
    UL(I,J) = 0.
    VL(I,J) = 0.
    WL(I,J) = 0.
    AL(I,J) = 0.
    BL(I,J) = 0.
    CL(I,J) = 0.
    RESL(I,J) = 0.
    IF (KSYM.NE.0) GO TO 21
    CALL YSKEEP = 1.
    RV GO TO 51
21  DO 22 J=1,MY
    DO 22 I=1,MX
    G(I,J,2) = G(I,J,3)
    GL(I,J) = G(I,J,3)
22  REAC(N1,ERR=101) ((G(I,J,3),I=1,MX),J=1,MY)
    WRITE(N2) ((G(I,J,1),I=1,MX),J=1,MY)
    K = K + 1
31  GO TO 51
    CALL YSKEEP = 1.
    RV IF (K.NE.KTE2) OR (YAh.LE.0.) GO TO 51
    IO ITEI(K) + 1
    DO 42 I=10,LX
    M = NX + 2 - I
    V G(M,KY,1) -G(I,KY,1)
    NV = NV + 1
    VORT(NV) = VORT(NV) + P3*(V -VORT(NV))
42  VORT(NV) = VORT(NV) GO TO 61
51  IF (K.EC.K2) GO TO 61
    DO 52 J=1,MY
    DO 52 I=1,MX
    G(I,J,1) = G(I,J,2)
    G(I,J,2) = G(I,J,3)
52  REAC(N1,ERR=101) ((G(I,J,3),I=1,MX),J=1,MY)
    WRITE(N2) ((G(I,J,1),I=1,MX),J=1,MY)
    K = K + 1
61  GO TO 21
    DO 62 M=2,3
    WRITE(N2) ((G(I,J,M),I=1,MX),J=1,MY)
62  CONTINUE
    FRES/64.
    AGRES = AGRES/(64.*TOT)
    IO = 1
    RETURN = 0
101 IO

```


RETURN
ENC


```

R(I)      = 0.
QP(I)     = 0.
FU(I)     = 0.
FW(I)     = 0.
CG(I)     = 0.
XM(I)     = 0.
YM(I)     = 0.
XR1(I)    = 0.
XR2(I)    = 0.
YRM(I)    = 0.
ZRM(I)    = 0.
IF (S.GT.0.) T = .5*ATAN2(B,A)
IF (B.EC.0.) AND.YM(I).GT.(FS +FS) T = .5*PI
IF (B.EC.C.) SQRT(S)
YM(I)     = .5*YM(I) +S*SIN(T)
ZM(I)     = .5*ZM(I) +S*COS(T)
A         = .25*(ZRM(I)**2 -YRM(I)**2) +FS**2
B         = SQRT(A**2 +B**2)
S         = 0.
T         = .5*ATAN2(B,A)
IF (S.GT.0.) AND.YM(I).GT.(FS +FS) T = .5*PI
IF (B.EC.C.) SQRT(S)
YM(I)     = .5*YM(I) +S*SIN(T)
ZM(I)     = .5*ZM(I) +S*COS(T)
A         = .25*(ZRM(I)**2 -YRM(I)**2) +FS**2
B         = SQRT(A**2 +B**2)
S         = 0.
T         = .5*ATAN2(B,A)
IF (S.GT.0.) SQRT(S)
YRM(I)    = .5*YRM(I) +S*SIN(T)
ZRM(I)    = .5*ZRM(I) +S*COS(T)
DO 21  I=1,MX
X(I)      = XM(I)
Y(I)      = YM(I)
Z(I)      = ZM(I)
XR(I)     = XRM(I)
YR(I)     = YRM(I)
ZR(I)     = ZRM(I)
XM(I)     = X1*(A0(I)**2 -(B0(J+1) +S0(I,K))**2)
YM(I)     = S2*A0(I)*(B0(J+1) +SC(I,K))
ZM(I)     = SR1*(A0(I)**2 -(B0(J+1) +S0(I,K+1))**2)
XR1(I)    = SR2*A0(I)*(B0(J+1) +S0(I,K+1))
YR1(I)    = 0.
ZR1(I)    = 0.
IF (FUS.LE.C.) GO TO 31
DO 24  I=1,MX
A         = .25*(ZM(I)**2 -YM(I)**2) +FS**2

```



```

B S T I F (S.GT.0.) = .5*ZM(I)*YM(I)
IF (B.EC.0.) = 0.0 SQR T(A**2 +B**2)
IF (B.EC.0.) = 0.0 I = .5*ATAN2(B,A) +FS) T = .5*PI
S Y M(I) = .5*YM(I) +S*SIN(T)
Z M(I) = .5*ZM(I) +S*COS(T)
A B T S = .25*(ZRM(I)**2 -YRM(I)**2) +FS**2
I S = 0.0 SQR T(A**2 +B**2)
IF (S.GT.0.) T = .5*ATAN2(B,A)
S Y R M(I) = .5*YRM(I) +S*SIN(T)
Z R M(I) = .5*ZRM(I) +S*COS(T)
24 DO 32 I=1,NX
31 XX XR(I+1) +XR(I) +XRM(I+1) -XRM(I)
XY +X(I+1) -X(I) +XR(I+1) -XR(I)
XZ +X(I+1) +X(I) -X(I+1) -XR(I)
YX -Y(I+1) +Y(I) +YRM(I+1) -YRM(I)
YY +Y(I+1) +Y(I) -Y(I+1) -YRM(I)
YZ +Y(I+1) +Y(I) +YRM(I+1) -YRM(I)
ZX -Z(I+1) +Z(I) +ZRM(I+1) -ZRM(I)
ZY +Z(I+1) +Z(I) -Z(I+1) -ZRM(I)
ZZ -Z(I+1) +Z(I) +ZRM(I+1) -ZRM(I)
FX X -YZ**ZZ
FY X -YX**ZZ
FZ X -YX**ZY
FY Y -ZY**XZ
FZ Y -ZZ**XX
FX Z -ZY**XY
FY Z -XZ**YZ
FZ Z -XX**YY
FM(I) -FX**XX
A /FM(I)
GX G(I+1,J,2) -G(I,J,2) +G(I+1,J+1,2) -G(I,J+1,2)

```



```

GXR      G(I+1,J,3)      -G(I,J,3)      +G(I+1,J+1,3)      -G(I,J+1,3)
GY       G(I+1,J,2)      +G(I,J,2)      -G(I+1,J+1,2)      -G(I,J+1,2)
GXY      G(I+1,J,3)      +G(I,J,3)      -G(I+1,J+1,3)      -G(I,J+1,3)
GX YR    G(I+1,J,2)      +G(I,J,2)      -G(I+1,J+1,2)      -G(I,J+1,2)
GZ       G(I+1,J,3)      +G(I,J,3)      -G(I+1,J+1,3)      -G(I,J+1,3)
1        G(I+1,J,2)      +G(I,J,2)      -G(I+1,J+1,2)      -G(I,J+1,2)
ABCM(I)  GXY      +GY      +FYX*GY      +FZX*GZ)*A      +CA
BCM(I)   GXR      -GX      +FYY*GY      +FZY*GZ)*A      +SA
CAM(I)   GX YR   -GX      +FYZ*GY      +FZZ*GZ)*A      +SYAW
ABCM(I)  GXR      +GY      +W*W
GX       (FXXY*GX      +FXZ*W
GY       (FXZ*GX      +FYX*V      +FYZ*W
U        U*U      +V*V      +W*W
V        AA      -2*GGM(I)      +FXZ*W
W        ABS(FMACH2*AA)      +FYX*V      +FYZ*W
AA       FXX*U      +FXY*V      +FZZ*W
DM(I)    FXX*U      +FYZ*V      +FXZ*W
UM(I)    FXX**2      +FYY**2      +FYZ**2
VM(I)    FXX**2      +FYY**2      +FZZ**2
WM(I)    FXX**2      +FYY**2      +FZZ**2
AM(I)    FXX**2      +FYY**2      +FZZ**2
BM(I)    FXX**2      +FYY**2      +FZZ**2
CM(I)    FXX**2      +FYY**2      +FZZ**2
DM(I)    DM(I)*DM(I)*SQRT(DM(I))
DO       DM(I)*UM(I)
DO       DM(I)*VM(I)
UM(I)    DM(I)*WM(I)
VM(I)    DM(I)*AM(I)
WM(I)    DM(I)*EM(I)
AM(I)    DM(I)*CM(I)
BM(I)    DM(I)*FM(I)
CM(I)    DM(I)*BM(I)
FM(I)    DM(I)*AM(I)
ABM(I)   DM(I)*BCM(I)
BCM(I)   DM(I)*CAM(I)
CAM(I)   DM(I)*CM(I)
ABCM(I)  DM(I)*BM(I)
IF       (J.LT.2) GO TO 71
DO       GO TO 71
QQP(I)   +GCP(I-1)      +QQM(I)      +QQM(I-1)
FR       +FP(I-1)      +FM(I)      +FM(I-1)
UR       +UP(I)      +VM(I)      +VM(I-1)
WR       +WP(I)      +WM(I)      +WM(I-1)
QQ       +RESO(I)      +BV*(QQR      +QQQL(I,J)
F        +FR)      +FL(I,J)

```



```

U V W QQL(I,J)
FL(I,J)
UL(I,J)
VL(I,J)
WL(I,J)
AA(QA(I))
QA(I)
QP(I)
P(I)
C(I)
R(I)
FU(I)
FV(I)
FW(I)
IF(QA(I),LE,1)
NSUP
F
FUL(I)
FVV(I)
FWW(I)
GXV
GYZ
GZY
GXZ
F
FXV
FYZ
FZX
P(I)
Q(I)
R(I)
42 PF CONTINUE
DO 52 I=2,NX
AV
PB
PF
IF((FU(I))
A
1
+UL(I,J))
+VL(I,J))
+WL(I,J))
BV*(UR
BV*(VR
CV*(WR
QQR
QUR
UVR
WR
AAO
QQ/AA
16.*RESO(I)/(F*AA)
Q(I)
O.
O.
O.
A*U
F*U
F*ABS(V)
F*ABS(W)
IF(QA(I),LE,1)
NSUP
A*(I.
F*U*V
F*W*W
G(I+1,J,2)
G(I,J,2)
G(I,J,3)
G(I+1,J,2)
-G(I+1,J,2)
G(I+1,J,3)
G(I+1,J,3)
.25*V*GXV
F*V*W*GYZ
F*W*U*GZX
F*U*(I)*GXV
F*V*(I)*GYV
F*W*(I)*GZZ
=P(2)
DO 52 I=2,NX
RESC(I)*RV
PF
P(I)
+FU(I+1),LI,0)
UP(I)
+VP(I)
+UL(I,J)
+VL(I,J)
+WL(I,J)
+G(I,J,2)
+G(I,J,2)
+G(I,J,2)
-G(I-1,J,2)
-G(I-1,J,2)
-G(I-1,J,3)
-G(I-1,J,3)
-G(I-1,J,3)
+FXV
+FYZ
+FZX
+FXV
+FXV
+FYZ
+FYZ
+P(I+1)
+UM(I)
-VM(I-1)
-VM(I-1)
-VM(I)
-VM(I-1)

```



```

2 B      -ABP(I) +ABP(I-1) +ABM(I) -ABM(I-1)
1 1      -WP(I) +WP(I-1) +WM(I) +WM(I-1)
1 2      -BCP(I) -BCP(I-1) +BCM(I) +BCM(I-1)
3      +CAP(I) -CAP(I-1) +CAM(I) +CAM(I-1)
RES(I)  +ABC(I) -ABC(I) +ABCM(I) +ABCM(I-1) +R(I)
RESL(I,J) +AV*(A +B +PF -PB) +QP(I) -Q(I) +RESL(I,J)
AR      = A -B      +AP(I-1) +AM(I) +AM(I-1)
BR      = AP(I) +BP(I-1) +BM(I) +EM(I-1)
CR      = CP(I) +CP(I-1) +CM(I) +CM(I-1)
A       = AV*AR +AL(I,J)
B       = AV*ER +BL(I,J)
C       = AV*CR +CL(I,J)
AL(I,J) = AR
BL(I,J) = BR
CL(I,J) = CR
A       = A +B
B       = B +C
C       = C +A
TP      = A +Q1*(B +C) +Q2*(ABS(FU(I)) +FV(I) +FW(I))
TS      = A +Q2*FV(I)*CG(I)
1 F      = (C +G2*FW(I))*G(I,J,1) -GL(I,J)
IF (QA(I),LE,I) GC TG 53
IF FU(I) = 0
F TP      = TP +F
T TP      = T +3.*(F +FVV(I) +FW(I)) +F
S TP      = S +3.*(FVV(I)*CG(I) +Fw(I))*G(I,J,1) -GL(I,J)
53 TM     (FU(I),GE,0.) TM = TM +Q2*FU(I) +F +F
IF (FU(I),LT,0.) TP = TP -Q2*FU(I) +F +F
TM      = TM*RESO(I-1)
B       = I.*(RES(I) -TM*E(I-1))
D(I)    = B*TP
D(I)    = B*TP
52 IF (J,LT,JI,OR,K,LT,K1) GO TO 71
I CG(I+1) = I2
CG(I+1) = 0.
DO 62 M=2,I2
GL(I,J) = G(I,J,2) +E(I)*CG(I+1)
CG(I)    = D(I) +E(I)*CG(I+1)
G(I,J,2) = G(I,J,2) +CG(I)
TOI      = TOI +I.
AR      = ARS +ABS(RES(I))
IF (ABS(RES(I)),LE,ABS(FRES)) GO TO 63
FRES     = FRES
IRES     = I

```



```

JRES
63 KR AG (ABS(CG(I)),LE.ABS(DG)) GO TO 62
   = K AG +AES(CG(I))
   = I CG(I)
   = J
   = K
71 DO I=1,NX
   QQP(I)
   DPM(I)
   FPM(I)
   VPM(I)
   WPM(I)
   BPM(I)
   CPM(I)
   ABP(I)
   BCP(I)
   CAP(I)
72 ABCP(I)
   J
81 IF (J -KY) 21,81,101
   I2
   IF (ITEZ(K).EQ.MX) I2 = LX
   IF (ISYM.EQ.1) I2 = NX
   DD 82 I=1,NX
   IF (ISYM.EC.1) GO TO 83
   IF (IV(I,K).EQ.2.OR.IV(I+1,K).EQ.2) GO TO 83
   M
   QQM(I)
   DPM(I)
   FPM(I)
   VPM(I)
   WPM(I)
   BPM(I)
   CPM(I)
   ABM(I)
   BCM(I)
   CAM(I)
   ABCM(I)
83 QQM(I)
   CM(I)

```



```
G(M,KY,2) = 0.5*V  
G(LX,KY+1,2) = G(LX,KY-1,2)  
RETURN  
END
```



```

C**SUBROUTINE VELC**
SUBROUTINE SURFACE
CALCULATES G(161,18),ITE1(35),XO(35),YO(35),ZC(35),SCAL(35),
COMMON AO(161),BO(18),KTE1,KTE2,ISYM,KSYM,FUS,
1 NX,NY,NZ,KYAW,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,IO
COMMON/SPA/ XL(161,18),YL(161,18),ZL(161,18),
2 XR(161,18),YR(161,18),ZR(161,18),
3 RE SL(161,18)
COMMON /UVW/ SV(1),VV(161),WW(161),YP(1)
DIMENSION PI = 3.1415926535898
Q1 = 1.0 / (.7 * FMACH**2)
TI = 1.0 / (.7 * FMACH**2)
MX = 1.5
NMAX = 1.5
AV (KSYM.EQ.1.AND.K.EQ.KTE1) GO TO 1
NMAX = 2.25
AV = K
1 IF (K.NE.KTE1) GO TC 11
N CO 2 J=1,2
DO 2 I=1,MX
X(I,J) = 0.
Y(I,J) = 0.
Z(I,J) = 0.
XR(I,J) = 0.
YR(I,J) = 0.
ZR(I,J) = 0.
N XR S = XO(N)/SCAL(KTE1)
YR S = YO(N)/SCAL(KTE1)
ZR S = ZO(N)/SCAL(KTE1)
S1 = SCAL(N)/SCAL(KTE1)
S2 = 5*S2
S1 = FUS/SCAL(KTE1)
DO 12 J=1,2
M DO 12 I=1,MX
XL(I,J) = X(I,J)
YL(I,J) = Y(I,J)
ZL(I,J) = Z(I,J)
XL(I,J) = XR(I,J)

```



```

U V W M XX YX ZX GX GO IF M N XX XZ YX YZ ZX GX GZ GO TO 25
+ (FXX*GX +FYX*GY +FZX*GZ)*F +CA
+ (FXY*GX +FYY*GY +FZY*GZ)*F +SA
+ (FXZ*GX +FYZ*GY +FZZ*GZ)*F +SYAW
= U = V = W = M = XX = YX = ZX = GX = GO = IF = M = N = XX = XZ = YX = YZ = ZX = GX = GZ = GO
= (I,1) -X(I-1,1)
= Y(I,1) -Y(I-1,1)
= Z(I,1) -Z(I-1,1)
= G(I,J,2) -G(I-1,J,2)
GO TO 26
= 1
= X(I+1,1) -X(I,1)
= XY(I+1,1) -XL(I,1)
= Y(I+1,1) -Y(I,1)
= Z(I+1,1) -YL(I,1)
= G(I+1,J,2) -ZL(I,1)
= G(I,J,2) -G(I,J,1)
GO TO 27
= AV*L
= AV*V
= AV*h
U*U +V*V +W*h
SQRT(Q) +Q1*(1. +Q1*(1. -Q))
AMACH*SV(I)/SQRT(Q)
TIC*(Q*3.5 -I.)
SCAL(KTEL)*X(I,1)
ITE1(K)
ITE2(K)
SCAL(KTEL)*X(I,1,1)
XMAX
YMAX
DO 22 I=11,12
XMAX1(XMAX,XP(I))
XMIN1(XMIN,XP(I))
YMAX1(YMAX,YP(I))
YMIN1(YMIN,YP(I))
22 RETURN
32 END

```



```

**SUBROUTINE CPLCT**
SUBROUTINE CPLCT (I3,I4,FMACH,XP,YP,CP,SM,I1,I2,KPLOT)
PLCTS CF AT COMPUTATIONAL MESH POINTS
COMMON /PCKR/ PTCK
COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
1 COMMON /UVW/ UU(161), VV(161), WW(161)
COMMON /PRS/ XOCO(161)
COMMON /SFARE/ LINE(90), DUMY(10)
DIMENS ICN KCDE(2), XP(1), YP(1), CP(1), SM(1)
DATA IST/1H*/
NOI = C
IMIN = I1 + (I2 - I1)/2
CHC = XF(I1) - XP(IMIN)
2 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000

```


25 CONTINUE
RETURN
61C FORMAT (2F10.4, F7.4, F8.4, F7.4, 90A1)
END


```

C**SUBROUTINE INVRT6**
SUBROUTINE INVRT6
COMMON /PCKR/ FTCK
COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
1 DI PEN S I C N P(161,6), UT3(161),
EQUIVALENCE (XT3(1),P(1,1))
DO 30 J=1,6
DO 10 I=1,NCI
M=NOI-I+1
TEMP(M)=F(I,J)
CONTINUE
10 CONTINUE
P(I,J)=TEMP(I)
DO 20 I=1,NCI
CONTINUE
20 CONTINUE
30 CONTINUE
WRITE(6,100) (I,XT3(I),YT3(I),UT3(I),
1 WRITE(1),VT3(I),I=1,NOI)
RETURN
100 FORMAT(4H0 I , 1X,6HXI3(I),4X,6HYT3(I),4X,6HUT3(I),
1 2 6X,4F 1 , 1X,6HXT3(I),4X,6HYT3(I),4X,6HUT3(I),
3 4X,6HVT3(I),4X,6HZI3(I)//
4 (I4,1X,6GI0.3,2X,I4,1X,6GI0.3)
END

```



```

C**SUBROUTINE FCRCF*****
SUEROUTINE FORCE (I1,I2,XP,YP,CP,AL,CHCRD,XM,YM,CL,CD,CM)
CALCULATES SECTION FORCE COEFFICIENTS
DIMENSICN = 57.29513082
RAD = AL/RAD
ALPHA = 0.
CL = 0.
CD = 0.
CM = I2 -1
DO 12 I=11,N
DX = (XP(I+1) -XP(I))/CHORD
DY = (YP(I+1) -YP(I))/CHORD
XA = (.5*(XF(I+1) +XF(I)) -XM)/CHORD
YA = (.5*(YF(I+1) +YF(I)) -YM)/CHORD
CPA = (.5*(CP(I+1) +CP(I))
DCL = -CPA*DY
DCC = CL +DCC
CD = CD +DCC
CM = +DCD*YA -DCL*XA
DCL = CL*COS(ALPHA) -CD*SIN(ALPHA)
DCL = CL*SIN(ALPHA) +CD*COS(ALPHA)
12 CONTINUE
RETURN
END

```



```

C**SUBROUTINE TCTFOR**
SUBROUTINE TOTFOR(KTE1,KTE2,CHORD,SCL,SCD,SCM,XO,YPO,ZPO,
CALCULATES TOTAL FORCE COEFFICIENTS
DIMENSION SCL(1),SCD(1),SCM(1),XC(1),YC(1),ZPO(1),
SPAN = -ZPO(KTE1)
CL = 0.
CD = 0.
CMP = 0.
CMY = 0.
S = 0.
KTE1 = KTE1
QL(K) = CHORD(K)
QD(K) = CHORD(K)
QM(K) = SCL(K)*CHORD(K) - SCL(K)*XO(K) + SCD(K)*YPO(K)
11 DZ = 5*(ZPO(K+1) - ZPO(K))
AZ = 5*(ZPO(K+1) + ZPO(K))
PL(K+1) = CHORD(K+1)
PD(K+1) = CHORD(K+1)
PM(K+1) = SCM(K+1)*CHORD(K+1) - SCL(K+1)*XO(K+1) + SCD(K+1)*YPO(K+1)
1 CLA = DZ*(PL + CL)
CDA = DZ*(PD + QD)
CL = CL + CLA
CD = CD + CDA
CMP = CMP + DZ*(PM + QM)
CMY = CMY + AZ*CLA + AZ*CDA + DZ*(CHORD(K+1) + CHORD(K))
S = S + PL
QD = QD + PM
QM = QM + PM
K = K + 1
IF (K.LT.KTE2) GO TO 11
CL = CL / S
CD = CD / S
CMP = CMP * SPAN / S**2
CMY = (CMY + CMR) / (S * SPAN)
CMY = (CMY + CMY) / (S * SPAN)
RETURN
END

```



```

C**SUBROUTINE REFINE**
C SUBROUTINE REFINE**
C HALVES MESH SIZE**
C COMMON G(I,1), I8,3), S0(I161,35), VORT(115), ZV(115),
1 IV(161), I35), ITE1(35), ITE2(35),
2 AO(161), B0(18), XO(35), YC(35), Z0(35), SCAL(35),
3 NX, NY, NZ, KTE1, KTE2, ISYM, KSYM, FUS,
4 YAW, CYAW, SYAW, ALPHA, CA, SA, FMACH, N1, N2, N3, IO
MX NX +1
MY NY +1
MZ NZ +3
MXO NX/2 +1
MYC NY/2 +2
MZC NZ/2 +1
K 1
IF (KSYM.EQ.0) GC TC 11
MZO = NZ/2 +3
READ (N1, ERR=401) ((G(I,J,1), I=1, MXO), J=1, MYO)
K 2
11 READ (N1, ERR=401) ((G(I,J,1), I=1, MXC), J=1, MYO)
J JJ
I II
II II
G(I, JJ, 1) = I I G(I, J, 1)
I II
IF (I.GT.0) GO TO 31
J JJ
JJ JJ
IF (J.GT.0) GO TO 21
DO 42 J=1, KY, 2
DO 42 I=2, NX, 2
G(I, J, 1) = .5*(G(I+1, J, 1) + G(I-1, J, 1))
DO 54 I=2, NY, 2
DO 54 J=2, NX, 2
G(I, J, 1) = .5*(G(I, J+1, 1) + G(I, J-1, 1))
G(I, MY, 1) = 0.
G(1, NY, 1) = 0.
G(MX, NY, 1) = 0.
WRITE (N2) ((G(I, J, 1), I=1, MX), J=1, MY)
K
IF (K.LE.MZC) GC TC 11
REWIND N1
READ (N2, ERR=401) ((G(I, J, 1), I=1, MX), J=1, MY)
READ (N2, ERR=401) ((G(I, J, 3), I=1, MX), J=1, MY)

```



```

WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MY)
K
IF (KSYM.NE.0) K = 2
111 K = K + 1
DO 112 I=1,MY
DO 112 J=1,MX
112 G(I,J,2) = .5*(G(I,J,1) +G(I,J,3))
DO 122 M=2,3
WRITE (N1) ((G(I,J,M),I=1,MX),J=1,MY)
122 CONTINUE
CONJINUE GC TC 201
DO 132 J=1,MY
DO 132 I=1,MX
132 G(I,J,1) = G(I,J,3)
REAC (N1,ERR=401) ((G(I,J,3),I=1,MX),J=1,MY)
201 GO TO 111
REWIND N1
DO 202 M=1,3
REAC (N1,ERR=401) ((G(I,J,M),I=1,MX),J=1,MY)
202 CONTINUE
WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
TYAW = SYAW/CYAW
VORT(NV) = KTE1 - 1
VORT(NV) = 0.
K
IF (KSYM.NE.0) GO TC 251
211 N = .5*SCAL(K)
N = NV
I = MX 0 + 1
IF (K.LT.KTE1) OR (K.GT.KTE2) GO TO 231
11 I = ITE1(K)
12 I = ITE2(K)
DO 212 J=1,I2
G(I,KY+1,2) = NV + 1
212 NV = G(I,KY,2) +G(I,KY,2) -G(I,KY-1,2)
VORT(NV) = NV
N = NV
I = I1
IF (K.NE.KTE2) OR (YAW.LE.0.) GO TO 231
221 I = I + 1
M = NV + 2 - 1
NV = NV + 1
VORT(NV) = G(M,KY,2) -G(I,KY,2)
IF (I.LT.MX0) GC TO 221
231 I = I1 - 1
V = 0.

```



```

IF (IV(I,K).NE.1) GG TC 237
ZZ = ZO(K) -TYAW*(XO(K) +S1*AC(I)*A0(I))
IF (ZZ.GE.ZV(N-1)) GO TO 235
N = N -1
GO TO 233
233 = (ZZ -ZV(N-1))/(ZV(N) -ZV(N-1))
= A*VCR1(N) +(1. -A)*VCR1(N-1)
= NX +2 -1
235 G(I,KY+1,2) = G(M,KY-1,2) -V
G(M,KY+1,2) = G(I,KY-1,2) +V
237 IF (IV(I,K).NE.-1) GO TO 241
G(I,KY,2) = .5*G(I,KY,1) +.25*(G(I,KY,3) +G(M,KY,3))
IF (IV(I,K+1).L1.1)
1 G(I,KY,2) = .5*G(I,KY,3) +.25*(G(I,KY,1) +G(M,KY,1))
G(M,KY,2) = .5*G(I,KY,2) +G(I,KY-2,2)
G(I,KY-1,2) = .5*G(I,KY,2) +G(M,KY-2,2)
241 G(I,GT,1) GO TO 231
G(I,KY,2) = -.5*V
G(M,KY,2) = .5*V
251 K = K +1
IF (K.EG.MZ) GO TO 261
DO 252 I=1,MX
DO 252 J=1,MX
G(I,J,1) = G(I,J,2)
G(I,J,2) = G(I,J,3)
252 WRITE (N2) ((G(I,J,I),I=1,MX),J=1,MY)
READ (N1,ERR=401) ((G(I,J,3),I=1,MX),J=1,MY)
GO TO 211
261 VORT(NV+1) = 0.
DO 262 M=2,3
WRITE (N2) ((G(I,J,M),I=1,MX),J=1,MY)
262 CONTINUE
REWIND N1
REWIND N2
DO 302 K=1,MZ
READ (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MY)
WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MY)
302 CONTINUE = 1
IO RETURN = 0
401 RETURN = 0
ENC

```



```

C**SUBROUTINE SMGCC**
SUBROUTINE SMOC
SMCGTHS PCTENTIAL
COMMON
1 18,3) ,SO(161,35),VORT(115),ZV(115),
2 IV(161,35),ITE1(35),ITE2(35),
3 AO(161),BO(18),XO(35),YC(35),ZO(35),SCAL(35),
4 NX,NY,NZ,KTE1,KTE2,ISYM,KSYM,FUS,
   YAW,CYAW,SYAW,ALPHA,CA,SA,FNACH,N1,N2,N3,IO
   = NX +1
   = NY +1
   = NZ +2
   = 2
   = NZ
   = NZ +2
   = 1./6.
   = 1./6.
DO 2 L=1,3
READ (N1,ERR=51) ((G(I,J,L),I=1,MX),J=1,MY)
CONTINUE
WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
K = K1
11 K = K +1
DO 12 J=3,NY
DO 14 I=2,NX
14 G(I,J,1) =
   -FX -PY -PZ)*G(I,J,2)
   +.5*PX*(G(I+1,J,2) +G(I-1,J,2))
   +.5*PY*(G(I,J+1,2) +G(I,J-1,2))
   +.5*PZ*(G(I,J,3) +G(I,J,1))
   = G(I,J,2)
G(I,J,1) = G(MX,J,2)
DO 16 I=1,MX
G(I,1,1) = G(I,1,2)
G(I,2,1) = G(I,2,2)
G(I,KY,1) = G(I,KY,2)
G(I,MY,1) = G(I,MY,2)
16 WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
IF (K.EC.K2) GO TO 31
DO 22 J=1,MY
DO 22 I=1,MX
G(I,J,1) = G(I,J,2)
G(I,J,2) = G(I,J,3)
22 READ (N1,ERR=51) ((G(I,J,3),I=1,MX),J=1,MY)
GO TO 11
31 WRITE (N2) ((G(I,J,3),I=1,MX),J=1,MY)

```



```

REWIND N1
REWIND N2
DO 42 K=1,MZ
  READ (N2,ERR=51) ((G(I,J,1),I=1,MX),J=1,MY)
  WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MY)
42 CONTINUE
   = 1
   RETURN
51 IO
   = 0
   RETURN
   END

```



```

      FPP(I)  -FF(I)*V
      = (V  -U)/DS
      = U  (F(J)  -F(I))/[S  -DS*(V  +L  +U)/6.
      = U  I
      = I  -K
      IF (J  -N) 41,51,41
      I  FPPP(N)
      = N  -K
      = FPPP(I)
      FPP(N)  = B
      FP(N)   = DF  +D*(FPP(I)  +B  +B)/6.
      IND    = I
      IF (MDC) 81,81,61
      FPPP(J) = FQM
      = FPP(J)
      = J  +K
      = S(J)  -S(I)
      = FPP(J)
      = FPPP(I)  +.5*DS*(F(I)  +F(J)  -[S*DS*(U  +V)/12.])
      = U
      IF (J  -N) 71,81,71
      IF (INC.EG.1) GC 7C 90
      WRITET (6,85) INC,MDC, I,J,K,M, S(I),S(J),DS,E
      85  FORMAT (6HOCHECK,6I10,4G13.4/)
      86  WRITET (6,86) (S(I),F(I),I=M,N)
      9C  FORMAT (10G13.4)
      RETURN
      ENC

```



```

C**SUBROUTINE INTPL**
SUBROUTINE INTP**
INTERPOLATION USING TAYLOR SERIES - JAMES SCOTT
ADCS CCFRECTION FOR PIECEWISE CONSTANT FOURTH DERIVATIVE
IF MODE GREATER THAN 0
DIMENSION SI(1), FI(1), S(1), F(1), FPP(1), FPPP(1)
K K = (N - M) / K
I MI
MIN = NI
D = S(N) - SI(MI)
IF (D*(SI(NI)) - SI(MI)) 11,13,13
11 MIN = NI
13 KI = 21, 21, 15
IF (KI) 21, 21, 15
15 KI = 21, 21, 15
21 II = 0
IF (MODE) 31, 31, 23
31 I = 1
33 I = SI(I) + KI
35 I = -N
37 I = SI(I) + KI
IF (D*(S(I)) - S(I)) 33, 33, 37
J I = -K
SS (FPPP(I) - FPPP(J) + .25*SS*FPPP) / (S(J) - S(I))
FPP(I) + .5*SS*FF
FF (FPP(I) + .5*SS*FF)
FI(II)
IF (II)
41 RETURN
ENC

```



```

C**SUBROUTINE VERTEC*****
SUBROUTINE VERTEC(I1,I2,XCCD,CP,NRD,ZPC,FMACH,YA,AL,
1 SCL,SCD,SCM,K)
C
C SUBROUTINE FOR VERSATEC PLCTTING OF THE PRESSURE COEFFICIENT
C VS NON-DIMENSIONAL CHORD (X/C) FOR EACH SECTION OF THE FINAL
C MESH
C
C REAL PXC(165),PCP(165),XCLO(85),XCLO(85),CPLD(85),CPUP(85),CPUP(85),
1 XCCD(161),CP(161),ZPO(35),SCL(35),SCD(35),SCM(35),
2 FMACH,YA,AL
C INTEGER I,J,NUM,NUM1,I1,I2,NRD,K
C
C INITIALIZE ARRAYS AND DATA TO ZERO.
NUM = C.0
NUM1 = C.0
DO 10 I=1,165
PXC(I) = 0.0
PCP(I) = 0.0
10 CONTINUE
DO 20 J=1,85
XCLO(J) = 0.0
CPLD(J) = 0.0
XCUP(J) = 0.0
CPUP(J) = 0.0
20 CONTINUE
C
C READ IN X/C AND CP DATA INTO NEW ARRAY STARTING AT ARRAY
C ELEMENT NUMBER 1
DO 30 I=1,I2
PXC(I-I1) +1) = XCCD(I)
PCP(I-I1) +1) = CP(I)
30 CONTINUE
PXC(NRD) = 1.0
C
C PUT THE DATA INTO TWO ARRAYS ONE FOR THE LOWER SURFACE
C AND ONE FOR THE UPPER SURFACE
NUM = (NRD-1)/2
NUM1 = NUM + 1
DO 40 I=1,NUM1
XCLO(I) = PXC(I)
CPLD(I) = PCP(I)
40 CONTINUE
DO 50 J=NUM1,NRD
XCUP(J-NUM) = PXC(J)
CPUP(J-NUM) = PCP(J)
50 CONTINUE
C INITIALIZE THE VERSATEC PLCTTER SYSTEM

```



```

C CALL PLCTS (0.0,0.0,0.0)
C SCALE THE DATA TO AN 5.0 X 7.0 INCH SPACE
CALL SCALE (PXC,5.0,NRD,+1)
CALL SCALE (PCP,7.0,NRD,-1)
C DRAW THE X AND Y AXIS
CALL AXIS (1.0,2.0, X/C,-3.5,0.0,C,PXC(NRD+1),PXC (NRD+2))
CALL AXIS (1.0,2.0, PRESSURE COEFFICIENT (CF),25,
>7.0,C,90.0,PCP(NRD+1),PCP (NRD+2))
C PUT SCALE FACTORS INTO TWO ARRAYS FOR UPPER AND LOWER SURFACE
XCLOC(NUM1+1) = PXC (NRD+1)
XCLOC(NUM1+2) = PXC (NRD+2)
CPLC(NUM1+1) = PCP (NRD+1)
CPLC(NUM1+2) = PCP (NRD+2)
C
XCUP(NUM1+1) = PXC (NRD+1)
XCUP(NUM1+2) = PXC (NRD+2)
CPLUP(NUM1+1) = PCP (NRD+1)
CPLUP(NUM1+2) = PCP (NRD+2)
C
C PLCT THE DATA PCINTS
CALL NEWPEN (2)
CALL PLCT (1.0,2.0,-3)
CALL LINE (XCLOC,CPLC,NUM1,1,-1,3)
CALL LINE (XCUP,CPLUP,NUM1,1,-1,11)
C
C PLACE TITLE AT TOP OF PAGE
CALL NEWPEN (3)
CALL SYMBCL (1.25,7.5,0.2, SECTION CP DATA ,0.0,16)
CALL SYMBCL (1)
CALL SYMBCL (1.25,7.25,0.1,* = UPPER SLRFACE ,0.0,18)
CALL SYMBCL (1.25,7.0,0.1,* = LOWER SURFACE ,0.0,18)
C
C PLACE THE FCCTING INFORMATION ON PLOT
CALL NEWPEN (2)
CALL SYMBCL (0.0,0.0,-.75,C.1, SPAN STATION = ,0.0,15)
CALL SYMBCL (999.0,0.1,ZPO(K),C.0,+3)
CALL SYMBCL (0.0,-1.0,0.1,MACF ,0.0,6)
CALL SYMBCL (995.0,0.1,FMACH,0.0,+3)
CALL SYMBCL (2.0,-1.0,0.1,YAW,C.0,+3)
CALL SYMBCL (995.0,0.1,YA,0.0,+3)
CALL SYMBCL (4.0,-1.0,0.1,ADA ,0.0,5)
CALL SYMBCL (995.0,0.1,AL,0.0,+3)
CALL SYMBCL (0.0,-1.25,0.1,CCL ,0.0,6)
CALL SYMBCL (995.0,0.1,SCL (K),C.0,+3)
CALL SYMBCL (2.0,-1.25,0.1,CDC ,0.0,5)

```



```
CALL NUMBER (995., 999., 0.1, SCD(K), 0.0, +5)  
CALL SYMBCL (4.0, -1.25, 0.1, CM, 0.0, +5)  
CALL NUMBER (995., 999., 0.1, SCM(K), 0.0, +5)  
  
C   END   PLCTTING  
        CALL PLCT (0.0, 0.0, +955)  
        RETURN  
        END
```


APPENDIX F

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE INTERACTIVE PROGRAM FLO27IN

```

C** FLO27IN FGRTRAN--1C709/83 JACK PASCHALL AERO ENGINEERING C
C A PROGRAM TO INTERACTIVELY DEFINE A FINE AERODYNAMIC FLOW PROBLEM C
C THIS PROGRAM WRITES AN INPUT FILE "FLO27IN.A" TO THE USERS C
C A DISK SYSTEM WHICH CAN BE SUBSEQUENTLY EXECUTED FOR JOB CARD ENTRY AND C
C A BATCH SYSTEM EXECUTION. C
C** REAL C
C** TITLE(16), FMESH, FNX, FNY, FNZ, FPLOT, FIT(3), COVD(3), P10(3), C
C** FMACH, YA, AL, CCO, ZSYM, FNS, SWEEP, DIHED, FUS, ZS, XL, YL, CHORC, C
C** THICK, AT, FSEC, FN, YSYM, XP(16), YP(16), ZERG, SCWFN, SCWXP(67), C
C** SCXYYP(67), SYMFN, SYMXP(59), FPYP(31), F14FN, N572FN, N572XP(41), F14YP(47), C
C** N72YYP(41), FFP(31), LISFN, LISXP(49), LISYP(49), N10FN, C
C** N10YYP(33), N10YYP(37), N10YYP(45), N34YYP(45), N35FN, C
C** N35YYP(45), N64YYP(45), N16YYP(45), N63FN, C
C** N66YYP(45), N63YYP(51), N63AFN, N63AXP(51), N63AYYP(51), N64OFN, C
C** N64YYP(51), N64YYP(51), N64AFN, N64AXP(51), N64AYYP(51), N650FN, C
C** N65YYP(51), N65YYP(51), N65AFN, N65AXP(51), N65AYYP(51), N660FN, C
C** N66YYP(51), N66YYP(51) C
C** INTEGER I, IA, J, JA, JM, NI, FLAG, NUM, SCWNUM, SYMNUM, N57NUM, FPNUM, C
C** F14NUM, A7NUM, LISNUM, N10NUM, N34NUM, N35NUM, N64NUM, N65NUM, C
C** N16NUM, N63NUM, N64AN, N65AN, N66AN, N660N C
C** ** SUPERCRTICAL WING SECTION DATA ** ** ** **
C** DATA SCWXP/1, 0, 8043, 7654, 7335, 2987, 2184, 1727, 6575, 9522, 9361, 5038, 8713, 8382, C
C** 4293, 3683, 0150, 0096, 0055, 0028, 0006, 0000, 0006, 0028, C
C** 0055, 0096, 0150, 0204, 0335, 0645, 0942, 1218, 1727, C
C** 2184, 2987, 3683, 4293, 4835, 5322, 5764, 6174, 6575, C
C** 6962, 7335, 7694, 8043, 8382, 8713, 9038, 9361, 9522, C
C** 9683, 9853, 9937, 101, 0374, 0381, 0414, 0438, 0461, 0506, 0544, 0579, C
C** 0611, 0641, 0669, 0699, 0725, 0751, 0780, 0805, 0827, C
C** 0847, 0859, 0860, 0843, 0826, 0752, 0764, 0723, 0654, C
C** 0607, 0581, 0545, 0507, 0471, 0420, 0378, 0336, 0284, C
C** 0246, 0206, 0167, 0136, 0080, 0000, 0045, 0073, 0105, C
C** 0130, 0140, 0126, 0105, 0077, 0044, 0007, 0033, C
C** 0081, 0129, 0178, 0228, 0273, 0310, 0347, 0388, C
C** 0339, 0329, 0308, 0302, 0293, C

```



```

C *** **SYMMETRICAL WING SECTION DATA *** ** ** ** **
DATA SYMFA59.0/,SYMNUM/59/,
1 2 3 4 5 6 7
SYMFP/1.
.0000 .8500 .7500 .7000 .6500 .6000 .
.5500 .4000 .3000 .2500 .2000 .1500 .
.1250 .1000 .0750 .0500 .0250 .0150 .
.0050 .0025 .0000 .0000 .0100 .0200 .
.0350 .0500 .0750 .1000 .1250 .1500 .
.3500 .4000 .4500 .5000 .6000 .7000 .
.8000 .8500 .9000 .9500 .
SYMYP/ .0025 .0130 .0180 .0240 .0290 .0340 .0375 .0415 .
.0450 .0475 .0505 .0525 .0555 .0580 .0610 .0640 .
.0680 .0675 .0650 .0625 .0600 .0575 .0550 .0525 .
.0490 .0465 .0440 .0415 .0390 .0365 .0340 .0315 .
.0290 .0265 .0240 .0215 .0190 .0165 .0140 .
.0120 .0095 .0070 .0045 .0020 .0000 .
.0230 .0265 .0300 .0335 .0370 .0405 .
.0440 .0475 .0510 .0545 .0580 .0615 .
.0650 .0685 .0720 .0755 .0790 .0825 .
.0860 .0895 .0930 .0965 .0995 .1025 .
.1055 .1085 .1115 .1145 .1175 .1205 .
.1235 .1265 .1295 .1325 .1355 .1385 .
.1415 .1445 .1475 .1505 .1535 .1565 .
.1595 .1625 .1655 .1685 .1715 .1745 .
.1775 .1805 .1835 .1865 .1895 .1925 .
.1955 .1985 .2015 .2045 .2075 .2105 .
.2135 .2165 .2195 .2225 .2255 .2285 .
.2315 .2345 .2375 .2405 .2435 .2465 .
.2495 .2525 .2555 .2585 .2615 .2645 .
.2675 .2705 .2735 .2765 .2795 .2825 .
.2855 .2885 .2915 .2945 .2975 .3005 .
.3035 .3065 .3095 .3125 .3155 .3185 .
.3215 .3245 .3275 .3305 .3335 .3365 .
.3395 .3425 .3455 .3485 .3515 .3545 .
.3575 .3605 .3635 .3665 .3695 .3725 .
.3755 .3785 .3815 .3845 .3875 .3905 .
.3935 .3965 .3995 .4025 .4055 .4085 .
.4115 .4145 .4175 .4205 .4235 .4265 .
.4295 .4325 .4355 .4385 .4415 .4445 .
.4475 .4505 .4535 .4565 .4595 .4625 .
.4655 .4685 .4715 .4745 .4775 .4805 .
.4835 .4865 .4895 .4925 .4955 .4985 .
.5015 .5045 .5075 .5105 .5135 .5165 .
.5195 .5225 .5255 .5285 .5315 .5345 .
.5375 .5405 .5435 .5465 .5495 .5525 .
.5555 .5585 .5615 .5645 .5675 .5705 .
.5735 .5765 .5795 .5825 .5855 .5885 .
.5915 .5945 .5975 .6005 .6035 .6065 .
.6095 .6125 .6155 .6185 .6215 .6245 .
.6275 .6305 .6335 .6365 .6395 .6425 .
.6455 .6485 .6515 .6545 .6575 .6605 .
.6635 .6665 .6695 .6725 .6755 .6785 .
.6815 .6845 .6875 .6905 .6935 .6965 .
.6995 .7025 .7055 .7085 .7115 .7145 .
.7175 .7205 .7235 .7265 .7295 .7325 .
.7355 .7385 .7415 .7445 .7475 .7505 .
.7535 .7565 .7595 .7625 .7655 .7685 .
.7715 .7745 .7775 .7805 .7835 .7865 .
.7895 .7925 .7955 .7985 .8015 .8045 .
.8075 .8105 .8135 .8165 .8195 .8225 .
.8255 .8285 .8315 .8345 .8375 .8405 .
.8435 .8465 .8495 .8525 .8555 .8585 .
.8615 .8645 .8675 .8705 .8735 .8765 .
.8795 .8825 .8855 .8885 .8915 .8945 .
.8975 .9005 .9035 .9065 .9095 .9125 .
.9155 .9185 .9215 .9245 .9275 .9305 .
.9335 .9365 .9395 .9425 .9455 .9485 .
.9515 .9545 .9575 .9605 .9635 .9665 .
.9695 .9725 .9755 .9785 .9815 .9845 .
.9875 .9905 .9935 .9965 .9995 .

```

```

C *** **NACA 24-30-0 SECTION DATA *** ** ** ** **
DATA N572FN/41.0/,N57NUM/41/,
1 2 3 4 5
N572YP/ .0013 .0120 .0204 .0376 .0515 .0642 .0730 .0780 .0788 .
.0768 .0726 .0661 .0563 .0414 .0350 .0290 .0220 .0128 .
.0070 .0050 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .
.0268 .0302 .0375 .0422 .0422 .0422 .0412 .0358 .
.0320 .0260 .0215 .0150 .0082 .0048 .0013 /

```

```

C *** **FLAT PLATE DATA *** ** ** ** **
DATA FFFN/31.0/,FPNLM/31/,
1 2 3 4
FFXP/1.
.0000 .5000 .0300 .0250 .0200 .0150 .0100 .0075 .0050 .0050 .
.0025 .0020 .0015 .0010 .0005 .0005 .0005 .0005 .0005 .
.0010 .0015 .0020 .0025 .0030 .0035 .0040 .0045 .0050 .
.0250 .0300 .0350 .0400 .0450 .0500 .0550 .0600 .0650 .
.0700 .0750 .0800 .0850 .0900 .0950 .1000 .1050 .1100 .
.1150 .1200 .1250 .1300 .1350 .1400 .1450 .1500 .1550 .
.1600 .1650 .1700 .1750 .1800 .1850 .1900 .1950 .2000 .
.2050 .2100 .2150 .2200 .2250 .2300 .2350 .2400 .2450 .
.2500 .2550 .2600 .2650 .2700 .2750 .2800 .2850 .2900 .
.2950 .3000 .3050 .3100 .3150 .3200 .3250 .3300 .3350 .
.3400 .3450 .3500 .3550 .3600 .3650 .3700 .3750 .3800 .
.3850 .3900 .3950 .4000 .4050 .4100 .4150 .4200 .4250 .
.4300 .4350 .4400 .4450 .4500 .4550 .4600 .4650 .4700 .
.4750 .4800 .4850 .4900 .4950 .5000 .5050 .5100 .5150 .
.5200 .5250 .5300 .5350 .5400 .5450 .5500 .5550 .5600 .
.5650 .5700 .5750 .5800 .5850 .5900 .5950 .6000 .6050 .
.6100 .6150 .6200 .6250 .6300 .6350 .6400 .6450 .6500 .
.6550 .6600 .6650 .6700 .6750 .6800 .6850 .6900 .6950 .
.7000 .7050 .7100 .7150 .7200 .7250 .7300 .7350 .7400 .
.7450 .7500 .7550 .7600 .7650 .7700 .7750 .7800 .7850 .
.7900 .7950 .8000 .8050 .8100 .8150 .8200 .8250 .8300 .
.8350 .8400 .8450 .8500 .8550 .8600 .8650 .8700 .8750 .
.8800 .8850 .8900 .8950 .9000 .9050 .9100 .9150 .9200 .
.9250 .9300 .9350 .9400 .9450 .9500 .9550 .9600 .9650 .
.9700 .9750 .9800 .9850 .9900 .9950 .

```

```

C *** **F-14 WING SECTION - TYPICAL *** ** ** ** *
DATA F14FN/47.0/,F14NUM/47/,
1 2
F14XP/1.
.2571 .2000 .1429 .0857 .0571 .0286 .0171 .0114 .
.8857 .7714 .6571 .5429 .4857 .4286 .3714 .3143 .

```



```

0057, .0029, .0016, .0005, .0000, .0010, .0020,
0029, .0014, .0117, .0229, .0286, .0571, .0857, .1429,
2000, .2571, .3143, .3714, .4286, .4857, .5429, .6571, .7714,
.8857, 1.0000,
F14VF/ .0000, .0166, .0320, .0451, .0549, .0571, .0574, .0574, .0573,
.0560, .0514, .0457, .0343, .0280, .0185, .0171, .0143, .0114,
.0076, .0046, .0036, .0023, .0015, .0000, .0013, .0017, .0017,
-.0028, -.0037, -.0059, -.0091, -.0115, -.0137, -.0160, -.0202,
-.0240, -.0289, -.0343, -.0366, -.0375, -.0375, -.0366, -.0343,
-.0301, -.0229, -.0142, -.0059, .0000/

```

```

C***A-7 WING SECTION - TYPICAL***
C***DATA A7FN/33.0 / A7NUM/33/***
1 2 3 4 1 2 3 4 5
C000, .8000, .6000, .4300, .3000, .2000, .1000, .0750, .0500,
C025, .0125, .0075, .0050, .0025, .0015, .0010, .0000, .0010,
.0015, .0025, .0050, .0075, .0125, .0250, .0500, .0750, .1000,
2C00, .3000, .4300, .6000, .8000, 1.0000,
A7VF/ .0000, .0163, .0320, .0451, .0549, .0571, .0574, .0574, .0573,
-.0031, -.0100, -.0146, -.0170, -.0185, -.0203, -.0213,
-.0219, -.0245, -.0265, -.0270, -.0277, -.0283, -.0289, -.0293,
-.0313, -.0329, -.0337, -.0339, -.0339, -.0335, -.0289, -.0330,
-.0350, -.0301, -.0163, .0000/

```

```

C***LIS SAMAN 7769 AIRFOIL SECTION***
C***DATA LISFN/49.0 / LISNUM/49/***
1 2 3 4 5 6 1 2 3 4 5 6
C000, .9500, .9000, .8000, .7000, .6000, .5000, .4000, .3000,
2C00, .1500, .1000, .0750, .0500, .0350, .0250, .0175, .0125,
C075, .0050, .0025, .0025, .0025, .0025, .0025, .0025, .0025,
.0020, .0025, .0050, .0075, .0125, .0175, .0250, .0350, .0500,
.0750, .1000, .1500, .2000, .3000, .4000, .5000, .6000, .7000,
8C00, .9000, .9500, 1.0000,
LISVF/ .0000, .0041, .0084, .0181, .0316, .0486, .0696, .0897, .0992,
.0526, .0840, .0706, .0615, .0456, .0406, .0334, .0272, .0225,
.0171, .0140, .0102, .0094, .0070, .0055, .0040, .0031, .0025,
-.0070, -.0080, -.0124, -.0137, -.0164, -.0182, -.0201, -.0216,
-.0230, -.0230, -.0216, -.0176, -.0138, -.0106, -.0091, -.0075,
-.0060, -.0045, -.0030, -.0016, -.0008, .0000/

```

```

C***NACA 0010 AIRFOIL SECTION***
C***DATA NICFN/37.0 / NICNUM/37/***
1 2 3 4 5 6 1 2 3
C000, .5500, .9000, .8000, .7000, .6000, .5000, .4000, .3000,
2500, .2000, .1500, .1000, .0750, .0500, .0250, .0125, .0050,
C000, .0050, .0125, .0250, .0500, .0750, .1000, .1500, .2000,
2500, .3000, .4000, .5000, .6000, .7000, .8000, .9000, .9500,
1.0000,
NICVF/ .0010, .0010, .0120, .0218, .0305, .0380, .0442, .0485,
.0500, .0495, .0478, .0445, .0390, .0350, .0217, .0178,
.0157, .0058, .0000, -.0098, -.0157, -.0217, -.0296,

```


2000, 1500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
 0050, 0025, 0010, 0005, 0001, 0001, 0001, 0001,
 0075, 0100, 0125, 0150, 0200, 0250, 0300, 0350,
 3000, 4000, 5000, 6000, 7000, 8000, 9000, 9500, 10000,
 N66 YF / 00100, 01656, 02833, 03430, 04089, 04556, 04822,
 04578, 04178, 03856, 03400, 03089, 02730, 02380, 02011,
 01320, 00985, 00585, 00170, 00017, 00000, 00000,
 00480, 00308, 00170, 00017, 00000, 00000, 00000,
 02656, 03089, 03400, 03856, 04178, 04578, 04822,
 04956, 05000, 04889, 04300, 02833, 01656, 00100 /

C ***** NACA 16-005 SECTION DATA *****
 DATA N16FN/45.0 / N16NUM/45 /, 8000, 7000, 6000, 5000, 4000, 3000,
 N16 XF / 1.0000, 9500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
 2000, 1500, 1000, 0750, 0500, 0025, 0010, 0005, 0001, 0001,
 0050, 0025, 0010, 0005, 0001, 0001, 0001, 0001,
 0075, 0100, 0125, 0150, 0200, 0250, 0300, 0350, 4000,
 3000, 4000, 5000, 6000, 7000, 8000, 9000, 9500, 10000,
 N16 YF / 00090, 01061, 01888, 03145, 03952, 04376, 04500, 04391,
 04063, 03498, 03101, 02553, 02274, 01882, 01354, 00969,
 00840, 00718, 00420, 00593, 00420, 00310, 00215, 00215,
 00300, 00420, 00420, 00593, 00718, 00840, 00969, 01354,
 01882, 02274, 02593, 03101, 03498, 04063, 04391,
 04500, 04376, 03952, 03145, 01888, 01061, 00090 /

C ***** NACA 63-010 SECTION DATA *****
 DATA N63FN/51.0 / N63NUM/51 /, 8500, 7000, 6500, 6000,
 N63 XF / 1.0000, 9500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
 5500, 5000, 4500, 4000, 3500, 3000, 2500, 2000, 1500,
 1000, 0750, 0500, 0250, 0125, 0100, 0075, 0050, 0050,
 0075, 0125, 0250, 0500, 1000, 1500, 2000, 2500,
 3000, 3500, 4000, 4500, 5000, 5500, 6000, 6500, 7000,
 7500, 8000, 8500, 9000, 9500, 10000, 02166, 02712, 03234,
 N63 YF / 00000, 00214, 00604, 01088, 01618, 02166, 02712, 03234,
 03715, 04140, 04496, 04766, 04938, 05000, 04538, 04753,
 04445, 03994, 03362, 02950, 02440, 01756, 01275, 01004,
 00829, 00012, 00082, 00100, 00100, 00100, 00100, 00100,
 02950, 03362, 03762, 03994, 04140, 04445, 04753, 04938,
 04938, 03762, 03362, 02950, 02440, 01756, 01275, 01004,
 02166, 01618, 01088, 00604, 00214, 00000 /

C ***** NACA 63A010 SECTION DATA *****
 DATA N63AFN/51.0 / N63AN/51 /, 8500, 7000, 6500, 6000,
 N63A XF / 1.0000, 9500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
 5500, 5000, 4500, 4000, 3500, 3000, 2500, 2000, 1500,
 1000, 0750, 0500, 0250, 0125, 0100, 0075, 0050, 0050,
 0075, 0125, 0250, 0500, 1000, 1500, 2000, 2500,
 3000, 3500, 4000, 4500, 5000, 5500, 6000, 6500, 7000,
 7500, 8000, 8500, 9000, 9500, 10000, 02166, 02712, 03234,
 N63A YF / 00000, 00214, 00604, 01088, 01618, 02166, 02712, 03234,
 03715, 04140, 04496, 04766, 04938, 05000, 04538, 04753,
 04445, 03994, 03362, 02950, 02440, 01756, 01275, 01004,
 00829, 00012, 00082, 00100, 00100, 00100, 00100, 00100,
 02950, 03362, 03762, 03994, 04140, 04445, 04753, 04938,
 04938, 03762, 03362, 02950, 02440, 01756, 01275, 01004,
 02166, 01618, 01088, 00604, 00214, 00000 /

6 N63AYF/ .7500 .8000 .8500 .9000 .9500 1.000/ .02545 .03044 .03517,
 .00021 .00525 .01030 .01535 .02040 .02545 .02545 .03044 .03517,
 .03943 .04311 .04613 .04837 .04968 .04995 .04995 .04913 .04714,
 .04400 .03950 .03324 .02917 .02412 .01737 .01250 .00983,
 .00815 .00000 .00815 .00583 .01220 .01737 .02412 .0412,
 .02917 .03324 .03950 .04400 .04714 .04913 .04995,
 .04968 .04837 .04613 .04311 .03943 .03517 .03044,
 .02545 .02040 .01535 .01030 .00525 .00021/

C*** **NA CA 64-010 SECTION DATA*** **NA CA 64-010 SECTION DATA*** **NA CA 64-010 SECTION DATA*** **NA CA 64-010 SECTION DATA*** **NA CA 64-010 SECTION DATA***

DATA N640FN/51 .0/ N640N/51/ .
 1 N640XF/1 .5000 .5500 .5000 .8500 .7500 .7000 .6500 .6000,
 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
 .0075 .0125 .0250 .0500 .0750 .1000 .1500 .2000,
 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500,
 .7500 .8000 .8500 .9000 .9500 1.000/ .02281 .02827 .03345,
 .00000 .00248 .00671 .01176 .01722 .02281 .02827 .03345,
 .03820 .04238 .04586 .04843 .04988 .04980 .04864 .04635,
 .04302 .03842 .03221 .02827 .02343 .01701 .01250 .00985,
 .00820 .00000 .00820 .00589 .01220 .01701 .02343,
 .02826 .03221 .03842 .04238 .04586 .04843 .04988,
 .04988 .04843 .04586 .04238 .03820 .03345 .02827,
 .02281 .01722 .01176 .00671 .00248 .00000

C*** **NA CA 64A010 SECTION DATA*** **NA CA 64A010 SECTION DATA*** **NA CA 64A010 SECTION DATA*** **NA CA 64A010 SECTION DATA*** **NA CA 64A010 SECTION DATA***

DATA N64AFN/51 .0/ N64AN/51/ .
 1 N64AXF/1 .5000 .5500 .5000 .8500 .7500 .7000 .6500 .6000,
 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
 .0075 .0125 .0250 .0500 .0750 .1000 .1500 .2000,
 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500,
 .7500 .8000 .8500 .9000 .9500 1.000/ .02623 .03127 .03597,
 .00021 .00541 .01062 .01582 .02103 .02623 .03127 .03597,
 .04021 .04388 .04684 .04854 .04995 .04968 .04837 .04606,
 .04272 .03813 .03199 .02905 .02327 .01688 .01225 .00969,
 .00804 .00000 .00804 .00569 .01225 .01688 .02103 .02623,
 .02905 .03199 .03813 .04272 .04684 .04854 .04995,
 .04995 .04854 .04684 .04388 .04021 .03597 .03127,
 .02623 .02103 .01582 .01062 .00541 .00021/

C*** **NA CA 65-010 SECTION DATA*** **NA CA 65-010 SECTION DATA*** **NA CA 65-010 SECTION DATA*** **NA CA 65-010 SECTION DATA*** **NA CA 65-010 SECTION DATA***

DATA N650FN/51 .0/ N650N/51/ .
 1 N650XF/1 .5000 .5500 .5000 .8500 .7500 .7000 .6500 .6000,
 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
 .0075 .0125 .0250 .0500 .0750 .1000 .1500 .2000,
 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500,
 .7500 .8000 .8500 .9000 .9500 1.000/ .02500 .03000 .03500,
 .00000 .00500 .01000 .01500 .02000 .02500 .03000 .03500,
 .03000 .02500 .02000 .01500 .01000 .00500 .00000 .00000,
 .00000 .00500 .01000 .01500 .02000 .02500 .03000 .03500,
 .03000 .02500 .02000 .01500 .01000 .00500 .00000 .00000,
 .00000 .00500 .01000 .01500 .02000 .02500 .03000 .03500,
 .03000 .02500 .02000 .01500 .01000 .00500 .00000 .00000


```

7500, .8000, .8500, .9000, .9500, .1987, .02584, .03156, .03682,
N650YF/ .0000, .00306, .00810, .01385, .01987, .02584, .03156, .03682,
.04146, .04530, .04812, .04996, .04996, .04924, .04760, .04503,
.04142, .03666, .03040, .02677, .02177, .01574, .01169, .00932,
.00772, .0000, .00772, .00532, .01169, .01574, .02177,
.02647, .03040, .03666, .04142, .04503, .04760, .04924,
.04996, .04963, .04812, .04530, .04146, .03682, .03156,
.02584, .01987, .01385, .00810, .00306, .0000

```

```

C ***** **NACA 65A010 SECTION DATA***** ** ** ** **
DATA N65AFN/51 .C/, N65AN/51/,
N65AXP/1 .0C00, .5500, .9000, .8500, .7500, .7000, .6500, .6000,
.5000, .4500, .4000, .3500, .3000, .2500, .2000, .1500,
.1000, .0750, .0500, .0250, .0125, .0075, .0050, .0050,
.0075, .0125, .0250, .0500, .1000, .1500, .2000, .2500,
.3000, .3500, .4000, .4500, .5000, .5500, .6000, .6500, .7000,
.7500, .8000, .8500, .9000, .9500, .1.00/,
N65AYP/ .00021, .00604, .01188, .01771, .02352, .02912, .03432, .03859,
.04304, .04632, .04863, .04983, .04995, .04912, .04742, .04483,
.04127, .03658, .03040, .02658, .02182, .01623, .01183, .00928,
.00765, .0000, .00765, .00528, .01183, .01623, .02182,
.02658, .03040, .03658, .04127, .04483, .04742, .04912,
.04995, .04983, .04863, .04632, .04304, .03899, .03432,
.02912, .02352, .01771, .01188, .00604, .00211/

```

```

C ***** **NACA 66-010 SECTION DATA***** ** ** **~
DATA N66CFN/51 .C/, N66ON/51/,
N660XP/1 .0000, .9500, .9000, .8500, .8000, .7500, .7000, .6500, .6000,
.5500, .5000, .4500, .4000, .3500, .3000, .2500, .2000, .1500,
.1000, .0750, .0500, .0250, .0125, .0075, .0050, .0050,
.0075, .0125, .0250, .0500, .1000, .1500, .2000, .2500,
.3000, .3500, .4000, .4500, .5000, .5500, .6000, .6500, .7000,
.7500, .8000, .8500, .9000, .9500, .1.00/,
N660YF/ .0000, .00408, .01054, .01773, .02494, .03176, .03787, .04302,
.04665, .04865, .04971, .05000, .04953, .04832, .04636, .04363,
.04001, .03530, .02917, .02536, .02087, .01516, .01141, .00913,
.00757, .0000, .02917, .03530, .04001, .04363, .04665, .04832,
.04953, .05000, .04971, .04865, .04665, .04302, .03787,
.03176, .02494, .01773, .01054, .00408, .0000/

```

```

C----- FILE DEFINITIONS -----
C CALL FRICMS (' FILEDEF ', '5', 'TERM', ' ', 'FLO27', ' ',
C FILEDEF ('8', 'DISK', ' ',
C 'CATAIN', 'A')
C-----

```


C TITLE PAGE AND INSTRUCTIONS
C-----

```
CALL FRICMS ('CLRSCRN ' )  
WRITE (6,410)  
WRITE (6,410)  
WRITE (6,420)  
WRITE (6,430)  
WRITE (6,41C)  
WRITE (6,410)  
WRITE (6,440)  
WRITE (6,410)
```

C FIRST LINE INPUT DATA--DEFINE COMPUTATIONAL GRID
C-----

```
WRITE (6,450)  
WRITE (6,46C)  
READ (5,1000) TITLE  
CONTINUE  
WRITE (5,*) FMESH  
WRITE (6,48C)  
READ (5,*) FNZ  
WRITE (6,490)  
READ (5,*) FNY  
CALL FRICMS (' CLRSCRN ' )  
WRITE (6,500)  
READ (5,*) FNZ  
WRITE (6,510)  
READ (5,*) FPLOT
```

10

C SUMMARY OF FIRST LINE INPUT DATA
C-----

```
CALL FRICMS (' CLRSCRN ' )  
WRITE (6,52C)  
READ (5,*) ANS  
IF (ANS.EQ.2) GC TC 20  
WRITE (6,521)  
WRITE (6,522) FNZ,FNY,FNZ,FMESH,FPLOT  
WRITE (6,530)  
READ (5,*) ANS  
IF (ANS.EQ.1) GO TO 10  
20 CONTINUE
```

C SECOND, THIRD AND FORTH LINES INPUT DATA--ITERATION AND CONVERGENCE
C TOLERANCE FOR GRID. NUMBER OF LINES EQUAL TO M = FMESH
C-----

```
M = IFIX(FMESH)  
CALL FRICMS (' CLRSCRN ' )
```



```

WRITE (6,450)
DO I=1,M
  IF (I.EC.1) WRITE (6,541)
  IF (I.EC.2) WRITE (6,542)
  IF (I.EC.3) WRITE (6,543)
  WRITE (6,550)
  REAL (5,*) FIT(I)
  WRITE (6,560)
  REAL (5,*) CCVD(I)
  WRITE (6,570)
  REAL (5,*) P10(I)
  CALL FRICMS ('CLRSCRN ')

```

30 CONTINUE

C SUMMARY OF SECOND, THIRD AND FORTF LINES INPUT DATA
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,580)
READ (5,*) ANS
IF (ANS.GE.2) GO TO 40
  WRITE (6,581)
  WRITE (6,582) (FIT(I),COVD(I),P10(I)),I=1,M)
  WRITE (6,590)
  READ (5,*) ANS
  IF (ANS.EQ.1) GO TO 20

```

40 CONTINUE

C FIFTH LINE INPUT DATA--MACH NO., YAW ANGLE, ADA, SKIN FRICTION DRAG
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,450)
WRITE (6,600)
READ (5,*) FMACH
WRITE (6,610)
READ (5,*) YA
WRITE (6,620)
READ (5,*) AL
WRITE (6,630)
READ (5,*) CDO

```

C SUMMARY OF FIFTH LINE INPUT DATA
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,640)
READ (5,*) ANS
IF (ANS.GE.2) GO TO 50
  WRITE (6,641)
  WRITE (6,642) FMACH,YA,AL,CDO

```



```

WRITE (6,650)
REAC (5,#) ANS
IF (ANS.EQ.1) GO TO 40
50 CONTINUE
C-----
C SIXTH LINE INPUT DATA--WING PLANFORM SYMMETRY, NUMBER OF SECTIONS,
C SWEEP, DIHEDRAL ANGLE AND FUSELAGE RADIUS
C-----
CALL FRICMS (' CLRSCRN ')
WRITE (6,450)
WRITE (6,660)
READ (5,#) ZSYM
WRITE (6,670)
READ (5,#) FNS
WRITE (6,680) SWEEP
WRITE (6,690) DIHED
READ (5,#) DIHED
WRITE (6,700)
REAC (5,#) FUS
C-----
C SUMMARY OF SIXTH LINE INPUT DATA
C-----
CALL FRICMS (' CLRSCRN ')
WRITE (6,710)
READ (5,#) ANS
IF (ANS.GE.2) GO TO 60
WRITE (6,711) ZSYM,FNS,SWEEP,DIHED,FUS
WRITE (6,720)
READ (5,#) ANS
IF (ANS.EQ.1) GO TO 50
60 CONTINUE
C-----
C WRITE JCL CARDS TO TOP OF FILE ON USER'S "A" DISK
C-----
WRITE (8,1200)
WRITE (8,1210)
C-----
C WRITE FIRST SIX LINES OF DATA TO FILE ON USER'S "A" DISK
C-----
WRITE (8,1010) TITLE
WRITE (8,1020) FNX,FNY,FNZ,FMESH,FFLCT
WRITE (8,1030) ((FIT(I),COVD(I),P10(I)),I=1,M)
WRITE (8,1040)
WRITE (8,1050) FMACH,YA,AL,CDO
WRITE (8,1060)
WRITE (8,1070)

```



```
WRITE (8,1080)
WRITE (8,1090) ZSYM,FNS,SWEEP,CIHEC,FUS
```

C SECTION INFLT DATA

```
N = IFIX(FNS)
CALL FRTCMS (' CLRSCRN ')
WRITE (6,450)
WRITE (6,730)
WRITE (6,410)
```

```
DO I=1,N
  WRITE (6,760) I
  WRITE (6,770)
  REAC (5,*) ZS
  REAC (6,*) XL
  REAC (6,*) YL
  REAC (5,*) CFGRD
  REAC (6,*) THICK
  REAC (5,*) AT
  CALL FRTCMS (' CLRSCRN ')
  WRITE (6,830)
  REAC (5,*) FSEC
  WRITE (8,1110) ZS,XL,YL,CHORD,THICK,AT,FSEC
  IF (FSEC.EQ.0.0) GO TO 190
  CALL FRTCMS (' CLRSCRN ')
  WRITE (6,450)
  WRITE (6,740)
  WRITE (6,741)
  REAC (6,*) ANS
  FLAG = ANS
  IF (FLAG.GT.0) GO TO 70
  WRITE (6,840)
  REAC (5,*) YSYM
  CALL FRTCMS (' CLRSCRN ')
  WRITE (6,850)
  REAC (5,*) FN
```

C USER INPUT X AND Y COORDINATES FOR WING SECTION DEFINING GEOMETRY

```
NUM = IFIX(FN)
CALL FRTCMS (' CLRSCRN ')
```



```

180 WRITE (6,450) I
      WRITE (6,860) I
      DO 180 J=1,NUM
        WRITE (6,870) J
        READ (5,*) XP(J),YP(J)
        CONTINUE
      IF (YSYM .EQ. 0.0) GC TC 185
      NI = NUM
      JJ = NUM
      DO 183 IA=1,J1
        XP(NI-IA) = XP(IA)
        YF(NI-IA) = -YP(IA)
        CONTINUE
      NUM = NI + 1 (FN - 1.0)
      FN = FN
      CONTINUE
      WRITE (8,1120) FN
      WRITE (8,1130) FN
      WRITE (8,1140) FN
      WRITE (8,1150) ((XP(J),YP(J)),J=1,NUM)
      GO TO 190
      CONTINUE

```

70

C MENU INPUT X AND Y COORDINATES FOR WING SECTION DEFINING GEOMETRY
C -----

```

IF (FLAG .EQ. 1) GO TO 81
IF (FLAG .EQ. 2) GO TO 82
IF (FLAG .EQ. 3) GO TO 83
IF (FLAG .EQ. 4) GO TO 84
IF (FLAG .EQ. 5) GO TO 85
IF (FLAG .EQ. 6) GO TO 86
IF (FLAG .EQ. 7) GO TO 87
IF (FLAG .EQ. 8) GO TO 88
IF (FLAG .EQ. 9) GO TO 89
IF (FLAG .EQ. 10) GO TO 90
IF (FLAG .EQ. 11) GC TO 91
IF (FLAG .EQ. 12) GC TO 92
IF (FLAG .EQ. 13) GC TO 93
IF (FLAG .EQ. 14) GC TO 94
IF (FLAG .EQ. 15) GC TO 95
IF (FLAG .EQ. 16) GC TO 96
IF (FLAG .EQ. 17) GC TO 97
IF (FLAG .EQ. 18) GC TO 98
IF (FLAG .EQ. 19) GC TO 99
IF (FLAG .EQ. 20) GC TO 100
CONTINUE
WRITE (8,1120) FPFN
WRITE (8,1130) FPFN

```

81


```

WRITE (8,1140) ((FPXP(J),FPYP(J)),J=1,FPNUM)
GC TO 190
CCNTINUE
WRITE (8,1120) SYMFN
WRITE (8,1130)
WRITE (8,1140) ((SYMXP(J),SYMYP(J)),J=1,SYMNUM)
GC TO 190
CCNTINUE
WRITE (8,1120) SCWFN
WRITE (8,1130)
WRITE (8,1140) ((SCWXP(J),SCWYP(J)),J=1,SCWNUM)
GC TO 190
CCNTINUE
WRITE (8,1120) N572FN
WRITE (8,1130)
WRITE (8,1140) ((N572XP(J),N572YP(J)),J=1,N57NUM)
GC TO 190
CCNTINUE
WRITE (8,1120) F14FN
WRITE (8,1130)
WRITE (8,1140) ((F14XP(J),F14YP(J)),J=1,F14NUM)
GC TO 190
CCNTINUE
WRITE (8,1120) A7FN
WRITE (8,1130)
WRITE (8,1140) ((A7XP(J),A7YP(J)),J=1,A7NUM)
GC TO 190
CCNTINUE
WRITE (8,1120) LISFN
WRITE (8,1130)
WRITE (8,1140) ((LISXP(J),LISYP(J)),J=1,LISNUM)
GC TO 190
CCNTINUE
WRITE (8,1120) N10FN
WRITE (8,1130)
WRITE (8,1140) ((N10XP(J),N10YP(J)),J=1,N10NUM)
GC TO 190
CCNTINUE
WRITE (8,1120) N34FN
WRITE (8,1130)

```

82

83

84

85

86

87

88

89


```

98      WRITE (8,1140) ((N64AXP(J),N64AYP(J)),J=1,N64AN)
        GC TO 190
        CCNTINUE
        WRITE (8,1120) N650FN
        WRITE (8,1130)
        WRITE (8,1140) ((N650XP(J),N650YP(J)),J=1,N650N)
        GC TO 190
        CCNTINUE
        WRITE (8,1120) N65AFN
        WRITE (8,1130)
        WRITE (8,1140) ((N65AXP(J),N65AYP(J)),J=1,N65AN)
        GC TO 190
        CCNTINUE
        WRITE (8,1120) N660FN
        WRITE (8,1130)
        WRITE (8,1140) ((N660XP(J),N660YP(J)),J=1,N660N)
        GC TO 190
        CALL FRTCMS ('CLRSCRN ')
190     CONTINUE
200
C-----WRITE THREE LINES TO USER'S FILE INDICATING ENC OF CALCULATION
C-----
C-----WRITE JCL CARDS TO BOTTOM OF FILE CN USER'S "A" DISK
C-----
        WRITE (8,1160)
        WRITE (8,1170)
        WRITE (8,1180) ZERC
C-----
C-----INDICATE TC USER THAT INPUT IS COMPLETE
C-----
        CALL FRTCMS ('CLRSCRN ')
        WRITE (6,450)
        WRITE (6,880)
        WRITE (6,410)
        WRITE (6,890)
C-----FCRMT STATEMENTS
C-----
410     RETURN
        FORMAT (1X,79H=====)
1=====)

```



```

420 FORMAT (/,25X,24HFLO27 DATA INPUT PROGRAM,/,33X,7HAE-4501//)
430 FORMAT (8X,66HTHIS PROGRAM INTERACTIVELY WRITES A DATA FILE TO YOU
1R A DISK WHICH AM--FLO27,/)
440 2AL FLOW PROGRAM--FLO27,/)
1 FORMAT (/,8X,57HE NTER DATA FOR THE POTENTIAL FLOW PROGRAM IN FREE
2AL,/,8X,52H AFTER EACH QUESTION THE FORMAT IS GIVEN: (R) -RE
3R,/,8X,14H(1) - INTEGER,/,8X,45FEXAMPLE: (R,R) INPUT 2.5,6.789
450 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
460 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
470 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
480 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
490 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
500 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
510 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
520 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
521 1R,/,8X,14H(1) - INPUT 5,/)
522 1R,/,8X,14H(1) - INPUT 5,/)
530 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
541 1R,/,8X,14H(1) - INPUT 5,/)
542 1R,/,8X,14H(1) - INPUT 5,/)
543 1R,/,8X,14H(1) - INPUT 5,/)
550 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
2R,/,8X,14H(1) - INPUT 5,/)
3R,/,8X,14H(1) - INPUT 5,/)
560 1R,/,8X,14H(1) - INPUT 5,/)
1R,/,8X,14H(1) - INPUT 5,/)
570 1R,/,8X,14H(1) - INPUT 5,/)
2R,/,8X,14H(1) - INPUT 5,/)
3R,/,8X,14H(1) - INPUT 5,/)

```



```

580 FORMAT (1X,55H SUMMARY CF SECOND, THIRD AND FORTH LINES OF INPUT DA
1TA?/,1X,25H=> ENTER 1 = YES; 2 = NO)
581 FORMAT (1X,3HF IT,7X,4HCOVO,6X,3HP10)
582 FORMAT (1X,F5.1,5X,F7.6,3X,F3.1)
583 FORMAT (/,1X,48HCF ANGE SECOND, THIRD AND FORTH LINES INPUT DATA?,
1/,1X,25H=> ENTER 1 = YES; 2 = NO)
600 FORMAT (1X,46H=> ENTER FREE STREAM MACH NUMBER (FMACH): (R))
610 FORMAT (1X,40H=> ENTER ANGLE IN DEGREES (VA): (R))
620 FORMAT (1X,46H=> ENTER ANGLE COEFFICIENT IN DEGREES (AL): (R))
630 FORMAT (1X,58H=> ENTER DRAG COEFFICIENT DUE TO SKIN FRICTION (CDO
1): (R),/,5X,48H (UNLESS OTHERWISE AVAILABLE C.O1 IS RECOMMENDED))
640 FORMAT (1X,33H SUMMARY CF FIFTH LINE INFLT DATA?/,1X,25H=> ENTER
11 = YES; 2 = NO)
641 FORMAT (1X,5HF MACH,5X,2HYA,8X,2HAL,8X,3FCDO1)
642 FORMAT (1X,F4.2,6X,F3.1,7X,F8.6,/,/)
650 FORMAT (1X,29HCF ANGE FIFTH LINE INPUT DATA?/,1X,25H=> ENTER 1 =
1YES; 2 = NO)
660 FORMAT (1X,52H=> ENTER WING PLANFORM SYMMETRY TRIGGER (ZSYM): (R)
1/,1X,41H0.0 = YAWED WING HAS NC SPANWISE SYMMETRY,/,1X,38H1.0 = S
2WEPT WING HAS SPANWISE SYMMETRY)
670 FORMAT (1X,78H=> ENTER NUMBER OF SECTIONS WHERE WING SECTION GEOM
1ENTRY IS DEFINED (FNS): (R),/,5X,53H (VALUE MUST BE > OR = 3.0, BUT
2NOT GREATER THAN 11.0))
680 FORMAT (1X,58H=> ENTER LEADING EDGE SWEEP ANGLE IN DEGREES (SWEEP
1): (R))
690 FORMAT (1X,48H=> ENTER DIHEDRAL ANGLE IN DEGREES (DIHED): (R))
700 FORMAT (1X,36H=> ENTER FUSELAGE RADIUS (FUS): (R),/,5X,33HNOTE: U
1SE 0.0 FOR WING-ALONE CASE)
710 FORMAT (1X,33H SUMMARY OF SIXTH LINE INPUT DATA?/,1X,25H=> ENTER
11 = YES; 2 = NO)
711 FORMAT (1X,4HZ SYM,6X,3HFNS,7X,5HSWEEP,5X,5HCIED,5X,3HFUS)
712 FORMAT (1X,F3.1,7X,F4.1,6X,F6.3,4X,F6.3,4X,F10.6,/,/)
720 FORMAT (1X,29HCF ANGE SIXTH LINE INPUT DATA?/,1X,25H=> ENTER 1 =
1YES; 2 = NO)
730 FORMAT (5X,66H THE NEXT SET OF INPUT DATA WILL BE REPEATED FOR EACH
1WING SHAPE SECTION,/,5X,63HX AND Y COORDINATES DEFINING THE WING SECTI
2IGN EDGE AND PROCEEDING ARCUND,/,5X,67HS STARTING WITH THE UPPER SURFACE TRAILI
3NG EDGE,/,5X,57HX AND Y COORDINATES ARE NORMALIZED WITH THE CHORD
4 LENGTH,/,5X,46HWING SELECTION DEFINING COORDINATES CAN BE INPUT, /
5FORMAT (28X,23H**WING SELECTION MENU**/,6X,34HO = USER INPUT SECTI
6ION COORDINATES, DATA,/,6X,19H1 = FLAT PLATE,/,6X,49H2 = SYMMETRICA
2L WING,/,6X,11X THICKNESS AT 30% CHORD),/,6X,61H3 = SUPERCritical WING (CA
3MBERED),/,6X,12X THICKNESS AT 32% CHORD),/,6X,51H4 = NACA 24-30 (CA
4MBERED),/,6X,52H5 = F14 WING (CAMBEREC,
59.5% CHORD),/,6X,66H6 = A-7 WING (7 DEG DR COP AT
620% CHORD),/,6X,7% THICKNESS AT 43% CHORD),/,6X,64H7 = LISSAMAN 7769 AI

```



```

741 7RFCIL (CAMBERED, 1, 1% THICKNESS AT 30% CHORD), /, 6X, 55H8 = NACA 0010
8 (SYMMETRICAL, 10% THICKNESS AT 30% CHORD), /, 6X, 58H9 = NACA 0010-3
94 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 59H10 = NACA 0010
>-35 (SYMMETRICAL, 10% THICKNESS AT 50% CHORD), /, 5X, 59H11 = NACA 00
110-64 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 59H12 = NACA
3A 16-00C (SYMMETRICAL, 19% THICKNESS AT 50% CHORD), /, 5X, 58H13 = NAC
4A 63-01C (SYMMETRICAL, 10% THICKNESS AT 35% CHORD), /, 5X, 58H15 = NA
5CA 63-A010 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 58H16 = N
6ACA 64-A010 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 58H17 = N
7NACA 65-A010 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 58H18 =
8 NACA 65-A010 (SYMMETRICAL, 10% THICKNESS AT 40% CHORD), /, 5X, 58H18 =
1 (CHORD), /, 5X, 58H20 = NACA 66-010 (SYMMETRICAL, 10% THICKNESS AT 45%
2 (CHORD), /, 5X, 58H20 = NACA 66-010 (SYMMETRICAL, 10% THICKNESS AT 45%
3 (CHORD), /, 5X, 58H20 = NACA 66-010 (SYMMETRICAL, 10% THICKNESS AT 45%
750 FORMAT (1X, 35H=> ENTER DESIRED NUMBER FROM MENU.)
760 FORMAT (15X, 22H***WING SECTION NUMBER, 12, 1X, 13HPARAMETERS***, /, 5X,
142HNOTE: ALL DIMENSIONS MUST BE IN SAME UNITS, //)
770 FORMAT (1X, 60H=> ENTER THE SPANWISE COORDINATE FOR THIS SECTION (
1ZS): (F))
780 FORMAT (1X, 53H=> ENTER SECTION LEADING EDGE X COORDINATE (XL): (R
1))
790 FORMAT (1X, 53H=> ENTER SECTION LEADING EDGE Y COORDINATE (YL): (R
1))
800 FORMAT (1X, 43H=> ENTER SECTION CHORD LENGTH (CHORD): (R))
810 FORMAT (1X, 55H=> ENTER SECTION THICKNESS SCALING FACTOR (THICK):
1 (R))
820 FORMAT (1X, 50H=> ENTER SECTION TWIST ANGLE IN DEGREES (AT): (R))
830 FORMAT (1X, 65H=> ENTER FLAG FOR DEFINING NEW WING SECTION GEOMETR
1Y (FSECT): (R), /, 1X, 40H1.0 = DEFINE A NEW WING SECTION GEOMETR
2X, 67H0.0 = COPY THE WING SECTION GEOMETRY FROM PREVIOUS S
3 SECTION, /, 7X, 38HNOTE: SECTION DEFINITION MUST ENTER 1.0)
840 FORMAT (1X, 44H=> ENTER FLAG FOR INDICATING WHETHER OR NOT, /, 5X, 43H
1THE WING SECTION IS SYMMETRICAL (YSYM): (R), /, 1X, 20H0.0 = ACNSYMME
2TRICAL, /, 1X, 25H1.0 = SYMMETRICAL SECTION, /, 1X, 53HNOTE: IF SYMMETRI
3CAL SECTION UPPER SURFACE.)
850 FORMAT (1X, 58H=> ENTER NUMBER OF WING SECTION DEFINING POINTS (FN
1): (R), /, 1X, 38HNOTE: MAXIMUM NUMBER OF POINTS IS 161.)
860 FORMAT (17X, 22H***WING SECTION NUMBER, 12, 1X, 22HX AND Y COORDINATES
1#*, //)
870 FORMAT (1X, 67H=> ENTER WING SECTION DEFINING POINT X AND Y COORD.
1 (XP, YP): (R, R))
880 FORMAT (5X, 64HTHREE ADDITIONAL DATA LINES WILL BE AUTOMATICALLY WR
1ITEN TO THE, /, 5X, 43HBOTTOM OF YOUR INPUT FILE. THESE LINES ARE: //
2, 5X, 18HEND OF CALCULATIONS, /, 5X, 38HFN, /, 5X, 38H0)
890 FORMAT (5X, 70HTHIS FILE HAS BEEN WRITTEN TO YOUR "A" DIS
1> <FILETYPE> FLG27, /, 5X, 69HDATA IN

```


2K. IF YOU WISH TO MAKE FURTHER CHANGES TO YOUR INPUT DATA
 3SI. APL YXEDIT THE CREATED DATA FILE.//,5X,62HCHANGES TO YOUR INPUT DATA
 4FLCk ENTER THE ADDITIONAL CARDS (JOB CARD ETC.).//,5X,61HXEDIT THE FILE
 5IN THE INSTRUCTIONS, THEN SUBMIT THE FILE TO THE,/,5X,60HAS CUTLINED
 70CESSOR.//,1X,4HBYE.)

```

1000 16(A4)
1010 1X,16(A4)
1020 3HFNX,5X,F4,1,6X,F4,1,6X,F3,1,7X,F3,1)
1030 3HFI,7X,4HCOVC,6X,3HP10)
1040 5,1,5X,F7,6,3X,F3,1)
1050 5HEMAC,5X,2HYA,8X,2HAL,8X,3HCCG)
1060 4,2,6X,F3,1,7X,F3,1,7X,F8,6)
1070 4HZSYM,6X,3HFNS,7X,5HSWEEP,5X,5HDIHED,5X,3HFUS)
1080 3,1,7X,F4,1,6X,F6,3,4X,F10,6)
1090 2HXS,8X,2HXL,8X,2HYL,8X,5HCHGRD,5X,5HTHICK,5X,
1100 12HAT,8X,4HFSEC)
1110 6(F8,4,2X),F3,1)
1120 2(FN)
1130 5,1)
1140 5HXP(1),5X,5HYP(1))
1150 6F10,7)
1160 1X,18HEND CF CALCULATION)
1170 3(FX)
1180 3,1)
1200 14H//GO.SYSIN DD *)
1210 17H//GO.SYSIN DD *)
1220 2H//)
1230 2H//)
  
```


LIST OF REFERENCES

1. Douglas Aircraft Company Report MDC J5519 (May 1973), A Theoretical Method for Calculating the Aerodynamic Characteristics of Arbitrary Jet-Flapped Wings, Second Edition 1977.
2. Cebeci, T. and Bradshaw, P., Momentum Transfer in Boundary Layers, McGraw-Hill Book Company, 1977.
3. McLean, J. D. and Randall, J. L., Computer Program to Calculate Three-Dimensional Boundary Layer Flows Over Wings with Wall Mass Transfer, NASA Contractor Report 3123, 1979.
4. Randall, J. L. and McLean, J. D., Computer Programs to Calculate Three-Dimensional Boundary Layer Flow Over Wings with Wall Mass Transfer, Program Maintenance Document, Vol. 1, NASA CR-158968, 1978.
5. Randall, J. L. and McLean, J. D., Computer Programs to Calculate Three-Dimensional Boundary Layer Flow Over Wings with Wall Mass Transfer, Program User's, NASA CR-158967, 1978.
6. Bogart, J. R., CDC to IBM FORTRAN IV Conversion Guide, Naval Postgraduate School W. R. Church Computer Center Technical Note No. MVS-04, August 1981.
7. Jameson, A. and Caughey, D. A., A Finite Volume Method for Transonic Potential Flow Calculations, AIAA Paper 77-635, 1977.
8. Anderson, R. F., Determination of the Characteristics of Tapered Wings, pp. 11, NACA Report 572, 1936

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0142 Naval Postgraduate School Monterey, California 93943	2
3. Department Chairman, Code 67 Department of Aeronautical Engineering Naval Postgraduate School Monterey, California 93943	1
4. Dr. Robert D. Zucker, Code 67Zu Department of Aeronautical Engineering Naval Postgraduate School Monterey, California 93943	5
5. Dr. Oscar Bitlarz, Code 67Bi Department of Aeronautical Engineering Naval Postgraduate School Monterey, California 93943	2
6. LCDR Lowell D. Boaz, Code 67Bo Department of Aeronautical Engineering Naval Postgraduate School Monterey, California 93943	2
7. CDR Jack Paschall III, Code 3107 Naval Weapons Center China Lake, California 93555	2

Thesis
P252
c.1

Thesis
P252
c.1

Paschall

2 0 7 4 2 4

A three-dimensional
transonic, potential
flow computer program,
its conversion to IBM
fortran and utilization.

9 APR 91

80517

207424

Thesis
P252
c.1

Paschall

A three-dimensional
transonic, potential
flow computer program,
its conversion to IBM
fortran and utilization.



thesP252

A three-dimensional transonic, potential



3 2768 001 98049 3

DUDLEY KNOX LIBRARY